

INSPIRING KIDS PRESERVE

THURSTON COUNTY, WASHINGTON

Project # 10181900021

Drainage and Erosion Control Plan

June 3, 2020

Prepared for:
Capital Land Trust
4405 7th Ave SE, Suite 306
Lacey, WA 98503

THURSTON COUNTY RECEIVED

SEP 18 2020

BUILDING DEVELOPMENT CENTER

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GHMMEDS

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Sageral West Constitution :

PROJECT ENGINEERS CERTIFICATION:

I hereby state that this Drainage and Erosion Control Plan/Construction SWPPP for Inspiring Kids Preserve has been prepared by me or under my supervision and meets the requirements of the Thurston County Drainage Design and Erosion Control Manual and the standard of care and expertise which is usual and customary in this community for professional engineers. I understand that Thurston County does not and will not assume liability for the sufficiency, suitability, or performance of drainage facilities prepared by me.



Capital Land Trust Inspiring Kids Preserve PROJECT # 10181900021

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1.0 PROJECT DESCRIPTION

1.1 Permits

Project may require the following permits from Thurston County:

- Conditional Use Permit
- Right-of-Way Permit
- Wetlands/Critical Areas Permit
- Forest Land Conversion
- SEPA
- Shoreline Permit.
- Grading Permit
- Construction Permit
- Building Permit
- On-Site Septic Approval
- Group B Water System Approval

1.2 Project Location

The project at is located at 4849 Johnson Point Road SE Olympia, Washington.

The project site is located on Thurston County Parcel Numbers: 11929110500, 11928220800, 11928230100, 11929140000, 11928230200, 11929440200, 11928320500, and 11928320000.

See Appendix A, Vicinity Map for project location.

The project location is situated between Johnson Point Road on the east and Henderson Inlet on the west. The property is currently undeveloped land owned by the Capital Land Trust.

1.3 Property Boundaries and Zoning

Parcels 11928230100, 11928230200, 11928320500, and 11928320000 are adjacent to Johnson Point Road.

See Appendices B and C Pre-Developed and Developed Site Conditions.

The parcels is zoned RRR 1/5 (Rural Residential/Recourse – One unit per five acre).

Under the RRR 1/5 zoning, educational facilities are allowed with a Special Use Permit. Maximum building coverage in this zone under a Special Use Permit is 20,000 square feet for parcels over ten acres in size. Hard surface limits for new construction in this zone is, for lots 2.5 acres and greater, ten percent.

Under Special Use provisions of TCC Title 20.54, the proposed site use is not listed as a specific Special Use. Per the pre-submittal meeting held with Thurston County, the County may find a similar permitted use and review the proposed use as similar to the permitted use. The County indicated that an Academic School (TCC 2.054.070(1) may be the most similar listed permitted use by a Special Use Permit. The project is subject to the specific and general standards of Title 20.54.

1.4 Project Description

The project site is a 112-acre nature preserve located off Johnson Point Road in northern Thurston County, including a mile of shoreline along Henderson Inlet. The purpose of the project is to facilitate the use of the nature preserve for educational purposes. Proposed improvements include a new access road, parking, a vehicle/bus turnaround loop, plaza, open air building, restroom with on-site septic system, Group B water system and access to site trails.

The new access from Johnson Point Road requires installation of a new culvert and construction of ingress and egress tapers consistent with Thurston County Road Standards for access to a major collector.

A 24-ft width, paved, access road with a paved 5-ft sidewalk along the north side will extend approximately 450-feet to a proposed bus/vehicle turnaround loop. A plaza area with a small (40-ft x 30-ft, 1200 sf) open air interpretive center building will be constructed at the far western end of the project.

The vehicle turnaround loop will provide access to the building and plaza as well as proposed interpretive trails. Two vehicle parking areas are proposed including an 8-stall parking area along the north side of the access road beginning about 75-ft from Johnson Point Road and a 16-stall parking area within the loop turnaround. Three handicap stalls will be provided. Vertical curbs will be provided along the roadway in front of the plaza area. In other areas, the sidewalk will be at grade to facilitate sheet flow runoff to dispersion areas.

Current plans not include a new well for water service and a small bathroom facility with associated on-site septic system.

The project area is approximately 1.4 acres and the site is currently undeveloped forest land with some isolated wetlands. The project proposes approximately 33,000 square feet of new impervious surfaces and 26,000 square feet of converted pervious surfaces.

1.5 Timing of the Project

It is anticipated that construction of the project will begin as soon as the Thurston County Construction Permit is obtained and is anticipated to be completed within 6 months of start of construction.

1.6 Summary of Core requirements

1.1.1 Core Requirement #1: Stormwater Site Planning

The project does not meet the criteria for an Abbreviated Drainage Plan and therefore requires a full Drainage and Erosion Plan (DECP) including a Drainage Report (this document), Construction SWPPP, Drawings and Specifications, and a Maintenance Plan.

1.1.2 Core Requirement #2: Construction Stormwater Pollution Plan

A full Construction SWPPP will be prepared as part of the final DECP and will be included in Appendix F.

1.1.3 Core Requirement #3: Source Control of Pollution

A source control plan will be prepared as part of the final DECP and will be included in Appendix G. Appendix G contains the source control checklist submitted with the Scoping Report.

1.1.4 Core Requirement #4: Preservation of Natural Drainage System and Outfalls

The project site consists of two Threshold Discharge Areas (TDAs) with about 60% of the developed area within the eastern TDA and the remaining 40% in the western TDA (see Appendix E, Stormwater Work Map). The project generally maintains the existing natural drainage patterns. Due to site grades, some small areas from the west TDA are routed to the east TDA; however, all drainage is dispersed to native vegetation and this minor diversion is inconsequential.

1.1.5 Core Requirement #5: On-site Stormwater Management

Core Requirement #5 will be met through the use of full dispersion in accordance with LID.11. Dispersion of runoff from the majority of impervious and converted pervious surfaces will be dispersed into at least 100-feet of native vegetation. A small area of the site (<5,000 sf impervious) will drain directly to Johnson Point Road and its adjacent ditch. Another small area (2,375 sf) near Johnson Point Road will sheet flow through between 25 and 100-ft of native vegetation before reaching the roadside ditch/wetland along Johnson Point Road.

Full dispersion is feasible because 65% of the site will remain in native conditions and impervious areas make up less than 10% of the site.

Dispersion of runoff will be through a combination of sheet flow dispersion directly from proposed roads and other impervious areas as well as multiple point discharges to rock pads and dispersion into a minimum of 100-ft of native vegetation. All point discharges will be for flows of less than 0.2 CFS.

1.1.6 Core Requirement #6: Runoff Treatment

With the exception of the small areas adjacent to Johnson Point Road, all impervious surfaces are fully dispersed in accordance with LID.11 therefore; the discharge of untreated stormwater into the ground is permitted.

For the area immediately adjacent to Johnson Point Road, runoff will either sheet flow down a fill embankment to the adjacent roadside ditch or flow to the south edge of the proposed new access apron and sheet flow to the new culvert outlet point. Runoff continues south in the roadside ditch toward a small wetland area within the subject property.

1.1.7 Core Requirement #7: Flow Control

With the exception of the area immediately adjacent to Johnson Point Road, all runoff from the site is fully dispersed in accordance with LID.11, which results in eliminating the flow control facility requirement. See CR #5 for description of dispersion facilities. The total impervious surface in the area of Johnson Point Road is less than 10,000 square feet and the increase in flow from the existing to the post-developed is less than 0.15 cfs (0.08 per WWHM), therefore this area is not subject to flow control

1.1.8 Core Requirement #8: Wetland Protection

Wetlands are present on the project site and on adjacent areas to the property. Discharges to dispersion areas at such that the dispersion flow path does not intersect most on-site wetlands within 100-feet. However, at the entrance from Johnson Point Road, two sub-basins discharge to a roadside wetland. The total impervious area of this discharge is less than 10,000 square feet and the discharge does not result in an increase in flows greater than 0.15 cfs (0.08 cfs, see Appendix D, WWHM Results) from the pre-developed conditions; therefore, the provisions of Core Requirement #8 do not apply to that discharge.

1.1.9 Core Requirement #9: Operation and Maintenance

An Operation and Maintenance Manual will be completed and recorded with the maintenance agreement prior to final project acceptance by Thurston County. Responsibility for operation and maintenance of the stormwater facilities will be by the property owner, Capital Land Trust.

1.1.10 Core Requirement #10: Financial Liability

Since there are no significant stormwater facilities for this project except point discharges to dispersion areas, and sheet flow, the applicant requests to be exempted from the financial liability requirement of the DDECM.

1.1.11 Core Requirement #11: Off-site Analysis and Mitigation

With the exception of the small area at the site entrance, all stormwater runoff will be fully dispersed on-site into at least 100-ft of native vegetation. Based on a review of site maps, Thurston County Geodata and a site visit by the project engineer, for the small area discharging to the Johnson Point Road ditch, it appears that the existing ditch along Johnson Point road drains to existing low areas and wetlands on the subject property and does not connect to any downstream receiving waters or conveyances. No known drainage problems occur in the vicinity of the project downstream from the property.

2.0 EXISTING SITE CONDITIONS

2.1 Site Topography

Site topography varies from relatively flat to slopes approaching 20 percent within the project limits.

Along the west side of Johnson Point Road there is a drop to the toe of the road embankment of about four to five feet, then, along the proposed road alignment, the ground rises for about 400 feet at slopes of five to six percent to a high-point at elevation 140. It then slopes down to the west at five to seven percent for about 200 feet. Beyond this the slope steepens to about 15 to 18 percent and in some locations up to about 20 percent at the far west end beyond the developed area.

2.2 Ground Cover

Vegetation consists of evergreen and deciduous trees, brush and some grassy open areas. By aerial photograph records it appears the site was logged, but not completely clear-cut, just prior to 2002 and has regrown since then. It also appears that tree replanting may have occurred around 2009. Dirt roads appear in aerial photographs from 2002 to 2009 but have now grown over due to lack of use.

There are known wetlands on the property, most are outside the proposed project limits. Two small wetlands are located north and south of the access from Johnson Point Road, a wetland mitigation plan is being prepared for impacts to those two wetlands due to construction of the access point. In areas of wetlands, typical wetland plants would be expected. A wetland delineation was conducted of wetlands which are mapped on the site plan and a wetlands report is available.

No known unique or sensitive vegetation occurs within the project limits.

2.3 Drainage

Drainage within the project area is split into two Threshold Discharge Areas (TDA). The developed area is split 60/40 between the eastern and western TDAs, respectively.

The eastern TDA drains southerly and easterly toward Johnson Point Road and the adjacent property to the south. Several small wetlands occur within this area both within and beyond the project limits and some drainage is to those wetlands.

The western TDA drains southerly and westerly toward Henderson Inlet located about 600 feet to the west of the westerly project limits. Runoff from the project area does not appear to discharge via any defined channels prior to reaching Henderson Inlet.

2.4 Soils

A geotechnical report was prepared for the site by Landau and Associates in March of 2020. A copy of the geotechnical report is included in Appendix I. Five test pits were excavated at the site to depth of between 12 and 15 feet on February 26, 2020. Locations are shown on the TESC plan sheet.

Subsurface conditions at the site are mapped as Vashon Till (Qgt), a highly compact mixture of low permeability clay, sand and gravel deposited directly by glaciation.

Soils underlying the surface conditions (6 to 10 inches of topsoil) are categorized into two units: Recessional Lacustrine and Glacial Till. The Recessional material was observed in all test pits and exhibits low bearing capacity and very low infiltration rates. The Glacial Till was observed in two test pits (TP-4 and TP-5). Cobbles were observed in one test pit (TP-4) and are often found in glacial deposits.

The geotechnical report indicates that perched groundwater was observed at 6-feet below ground surface at one test pit (TP-4), which is located near a small isolated wetland south of the project limits. No groundwater was located in any other test pits. A true groundwater table was not observed during site explorations.

The Natural Resources Conservation Service (NRCS) mapped soils within the project limits and into the proposed dispersion areas include Alderwood Gravelly Sandy Loam, 15 to 30 percent slopes (HSG B) and Kapowsin Silt Loam (HSG D), 3 to 15 percent slopes. The Kapowsin soils cover the majority of the proposed developed area of the site including the majority of the roadway and most of the dispersion areas. The Alderwood soils are located on the far west end of the project toward the end of the roadway and in the vicinity of the proposed plaza and building.

According to NRCS, both Alderwood and Kapowsin soils are moderately well drained with a low to moderately low infiltration rate (Ksat) of 0.00 to 0.06 in/hr. The geotechnical report indicates that site infiltration capacity is limited (0.05 in/hr).

The NRCS soils map and report for the site is included in Appendix H.

2.5 Critical Areas

The site has been assessed for critical area impacts based on review of the critical area maps available on the Thurston County Geodata website and it has been determined that there are several wetlands located throughout the parcel. Wetlands were delineated and a wetlands report prepared. A mitigation approach is proposed for the impact to the two small wetlands located immediately adjacent to Johnson Point Road. No other wetlands are within the limits of the proposed project improvements.

No other critical areas are identified within the limits of the proposed project improvements. Geologic hazard areas associated with marine bluffs and steep slopes are located approximately 800-ft to the southwest off the proposed project on adjacent land under separate ownership.

The area along Henderson Inlet, approximately 600-ft west of the proposed project area is subject to Shorelines regulations and is designated Conservancy shoreline. Development limitations within the Conservancy Shoreline generally begin when work occurs less than 200-ft from the shoreline.

2.6 Adjacent Areas

The project site abuts Johnson Point Road where a new access point will be constructed consistent with Thurston County Road Standards. Property to the south and downslope of the property is residential, with a single home on a large lot. The property is located over 500-feet south of the proposed developed area. Across Johnson Point Road to the east there are several single-family residences. Property immediately to the North is owned by the Capital Land Trust and north of that (over 1000-feet) is additional residential development on large lots.

2.7 Precipitation Records

Precipitation records within the WWHM 2012 model will be used for all stormwater analysis on this project.

2.8 Reports and Studies

The Henderson Inlet is subject to a TMDL. A Basin Plan for the Woodland Creek basin was prepared, but this project is outside of the study area of that Basin Plan. No additional requirements are known to apply to this project at this site based on existing studies and reports.

3.0 GEOTECHNICAL REPORT

See Appendix I for Geotechnical Report.

4.0 WELLS AND SEPTIC SYSTEMS

There are no wells or septic systems on the subject property or within the proposed development area. Wells and septic systems exist associated with the home to the south (>500-feet from the project area) and across Johnson Point Road to the east.

The site is not within the Well Head Protection Area of a public water system.

5.0 FUEL TANKS

There are no known fuel tanks (in-use or abandoned) on the project site.

6.0 ANALYSIS OF THE 100 YEAR FLOOD

The Federal Emergency Management Agency (FEMA) Floor Insurance Rate Map (FIRM) for the property shows a 100-year flood (1% annual probability) zone adjacent to Henderson Inlet. The flood zone is AE, with a flood elevation of 14. The project site is over 300-ft from the boundary of the flood zone and the lowest elevation of the project area is approximately 110 feet. A copy of the FEMA FIRM panel is included in Appendix J.

7.0 AESTHETIC CONSIDERATIONS FOR FACILITIES

The only facilities proposed are dispersion devices which will generally not be visible from the developed area of the project. No other aesthetic considerations are applicable for stormwater management on the project.

8.0 FACILITY SIZING AND OFF-SITE ANALYSIS

8.1 Basin Description and Areas

As described previously the project includes two Threshold Discharge Areas, an eastern TDA that includes about 60% of the developed area and a western TDA with about 40% of the developed area. The developed area is comprised of 13 separate sub-basins designated A through M. Each sub-basin is shown on the stormwater work map included in Appendix E. The areas of each sub-basin and the stormwater approach proposed for each is listed in Table 1.

TABLE 1: BASIN SUMMARY

| Sub-Basin | Area (sf) | Area (acres) | How Stormwater Managed |
|--------------------|--------------|-----------------|---|
| | | | (see Note) |
| Project Parcel | n/a | 29.33 | <u>-</u> |
| AREA DISTURBED | 59,000 | 1.36 | |
| NEW IMPERVIOUS | 32,800 | 0.75 | |
| CONVERTED PERVIOUS | 26,200 | 0.60 | - |
| Α | 4925 | 0.1096 | Drains to Johnson Pt Road Ditch |
| В | 2375 | 0.0545 | Sheet flow dispersion, 32 to 100' flow path |
| С | 3000 | 0.0689 | Mixed point discharge/sheet flow |
| D | 1925 | 0.0442 | Sheet flow dispersion, >100' flow path |
| E | 3550 | 0.0815 | Sheet flow dispersion, >100' flow path |
| F | 2400 | 0.0551 | Sheet flow dispersion, >100' flow path |
| G | 4200 | 0.0964 | Point discharge, >100' flow path |
| Н | 1500 | 0.0344 | Point discharge, >100' flow path |
| l | 5250 | 0.1205 | Sheet flow dispersion, >100' flow path |
| J | 4050 | 0.0930 | Point discharge, >100' flow path |
| K (Total) | 7900 | 0.1814 | Point discharge, >100' flow path |
| K (Impervious) | 4775 | 0.1096 | - |
| K (pervious) | 3125 | 0.0717 | |
| L | 5450 | 0.1251 | Point discharge, >100' flow path |
| M | 7175 | 0.1647 | Sheet flow dispersion, >100' flow path |

Note: WWHM 2012 modeling indicates that the contributing area to a point discharge can be up to 5,660 square feet of impervious surface and not exceed the 0.2 cfs threshold for a point discharge. Therefore, while some of the sub-basins above include pervious surfaces, they are not broken out if the total sub-basin areas is less than 5.500 sf.

8.2 Proposed BMP Design

Full Dispersion, BMP LID.11 is proposed for managing the majority of runoff from the parking areas, sidewalks and 2-lane driveway. The proposed impervious surface is less than 10% of the total parcel and over 65% of native vegetation will be retained. This site is owned by the Capital Land Trust as a preserve which ensures that future development

will be limited in extent and the native vegetation areas will remain at greater than 65% of the property.

Full dispersion will be obtained through the use of dispersion methods consistent with BMP LID.11 including sheet flow dispersion and concentrated flow dispersion. See drainage plan for location of dispersion devices. All sheet flow dispersion from the roadway will be across a 2-ft width of gravel beyond the roadway edge. All point discharges from swales will include a minimum 3-ft wide by 4-ft long by 6-inch deep quarry spall pad. Point discharges from pipes (2 locations) will include a quarry spall dispersion pad of 7-ft width by 8-ft length by 1-ft depth.

Two sub-basins drain to Johnson Point Road ditch without being fully dispersed. Basin A (4,925 sf) drains directly from the access apron and first part of the access road directly to the Johnson Point Road ditch. Basin B (2,375 sf) also drains to the Johnson Point Road ditch, but sheet flows across between 30 and 100-ft of native vegetation before arriving at the ditch or roadside wetland. Since the direct discharge is less than 5,000 square feet of impervious surface and the remaining 2,375 square feet is dispersed and not recollected prior to leaving the site, runoff treatment is not required for this discharge. The total impervious surface within this basin area is less than 10,000 square feet and the increase in flows from the pre-developed (existing) condition is less than 0.15 cfs (0.08) therefor flow control for this small area is not required, nor is wetland analysis required (CR #8).

No other aesthetic considerations are applicable for stormwater management on the project.

8.3 Off-site Analysis

With the exception of the small area (<5,000 sf) at the site entrance, all stormwater runoff will be fully dispersed on-site into at least 100-ft of native vegetation. Based on a review of site maps, Thurston County Geodata and a site visit by the project engineer, for the small area discharging to the Johnson Point Road ditch, it the existing ditch along Johnson Point road drains to the south to low areas on the subject property and does not connect to any downstream receiving waters or conveyances. No known drainage problems occur in the vicinity of the project downstream from the property.

9.0 UTILITIES

Electric service will be provided by Puget Sound Energy. An on-site water supply well will be developed to provide water service. A new on-site septic system will be developed to serve a small bathroom facility for the site. An existing overhead powerline runs along the west side of Johnson Point Road in the vicinity of the proposed new access road. No other underground utilities are known to exist along the west side of Johnson Point Road in the project vicinity.

10.0 COVENANTS, DEDICATIONS, EASEMENTS

There are no easements, dedications or covenants associated with this project. The proposed permanent dispersion areas will be shown on the site plans, and included in the O&M Plan which becomes part of the Agreement to Maintain executed with Thurston County and recorded against the property.

11.0 PROPERTY OWNERS ASSOCIATIONS ARTICLES OF INCORPORATIONS

There are no property owners associations associated with the project.



Scale 1: 85,903

0.5

VICINITY MAP

Legend

Roads - Major Major Roads - 15; US 101

AN GR NIVRAM

LIBBY RD NE

-- Ramp

Roads (Small Scale)

□ County Border

PROJECT SITE

BN QS

SHINCKE RD, NE

LIBBY RD NE

OINT, RD NE

MARVIN RD

+ Railroads

Map Created Using GeoData Public Website 6/2/2020

Note:

CARPENTER RD NE

SLEATER KINNEY, RD NE

REHINOS

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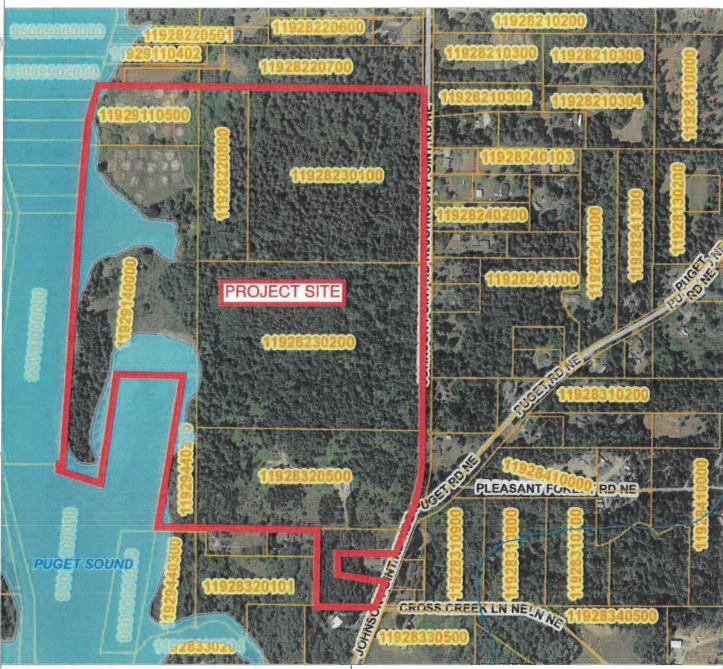
336TH AVE NE

LIBBY RD NE

Published:

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Legend

- Streams
- Waterbodies

Label - Parcel Number

Parcel Boundaries

Roads - Major

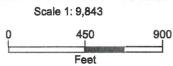
Major Roads

Ramp

15; US 101

Roads (Large Scale)

- Railroads
- County Rorder







Map Created Using GeoData Public Website

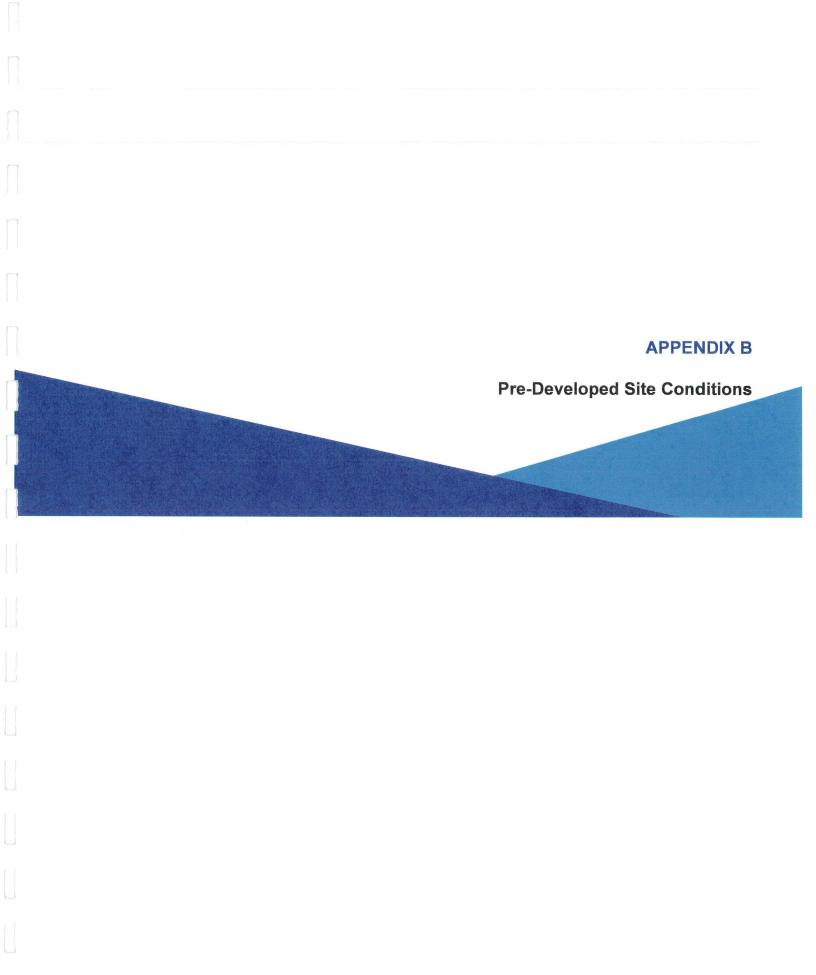
Published: 2/14/2019

Note: Existing topography not visible at this scale



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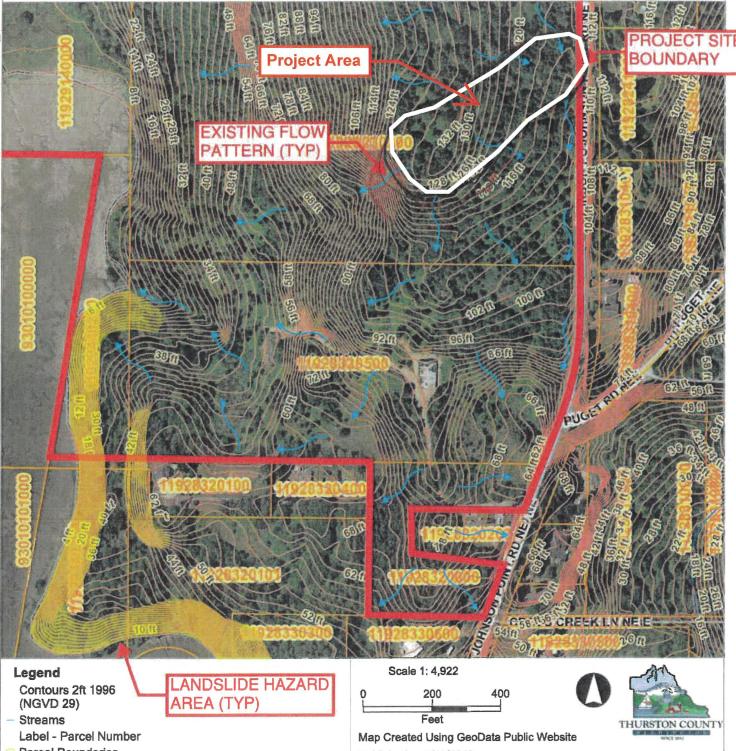
Map Created Using GeoData Public Website Roads (Large Scale) □ Building Footprints Parcel Boundaries Contours 2ft 1996 Published: 6/2/2020 □ County Border Roads - Major Scale 1: 5,369 Major Roads (NGVD 29) - 15; US 101 Wetlands + Railroads --- Ramp Note: NOSNHOP 9 NC NHOR 1102 (PROJECT AREA

11 09

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GeoData Center

EXISTING SITE CONDITIONS MAP



Parcel Boundaries

Roads - Major

Major Roads

Ramp

15; US 101

Roads (Large Scale)

→ Railroads

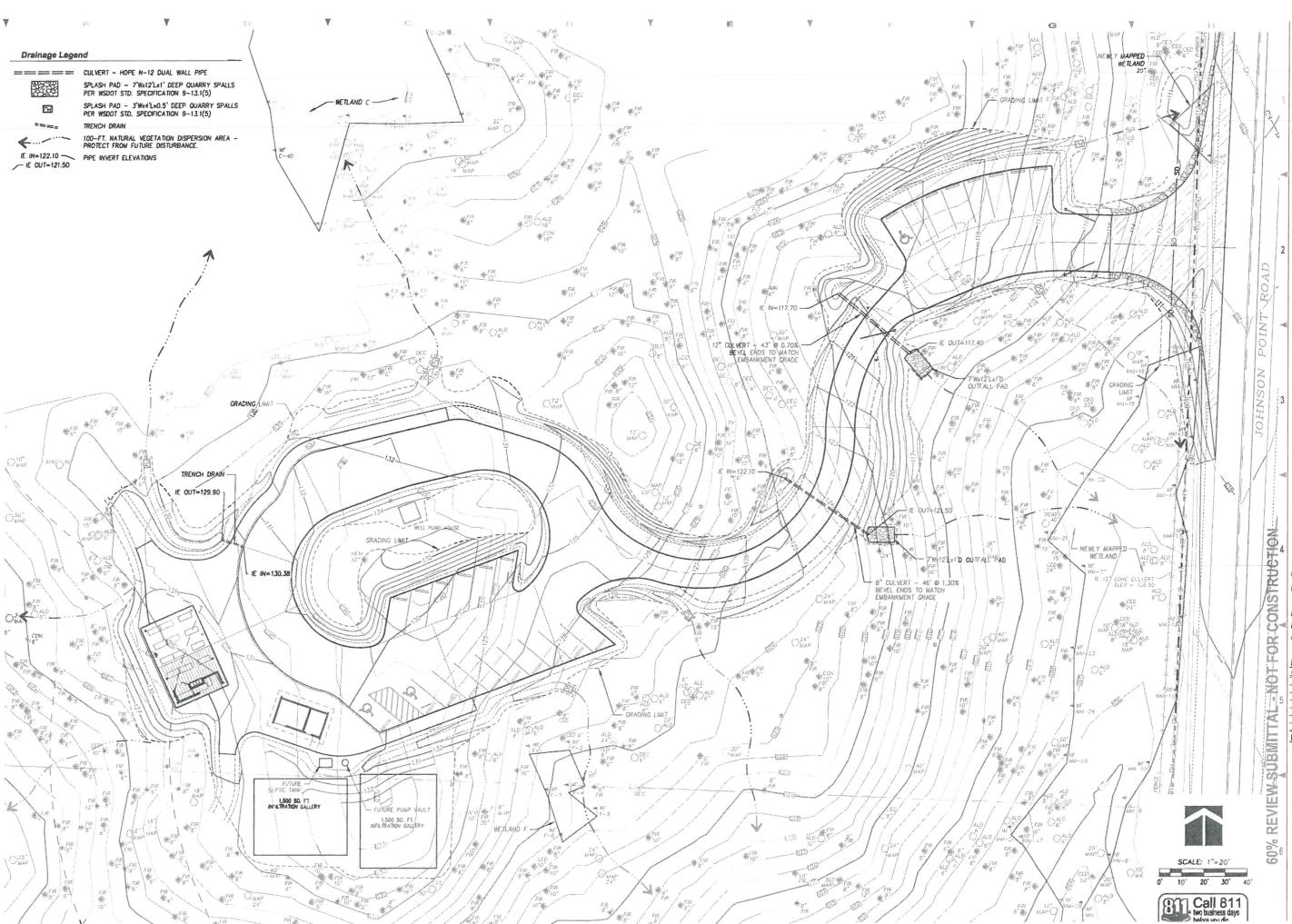
Published: 2/19/2019

Note:



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Inspiring K Preserve

Capitol Land Trust Lacey, WA

Robert W. Dr



05 7th Avenue SE, Ste.
Locey, WA 9
(360) 456FAX (360) 493E-MAIL bob@wdroli

Landscape Architec Site Plan Athletic Facility De Urbon De Land Plan



PROJECT NO. _____

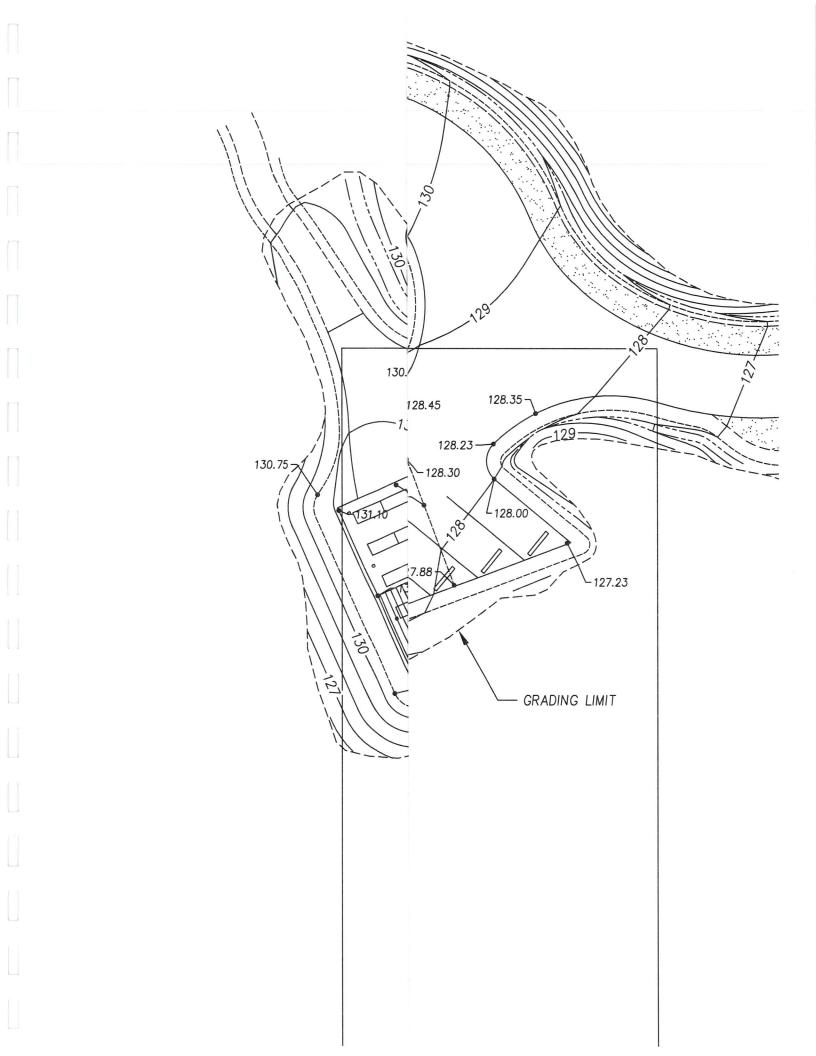
DESIGNED BY ______
DRAWN BY _____
CHECKED BY _____

DATE: MAY 22.

Drainage Pl

L4.0

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Attach WWHM 2012 Runs for the following:

0.2 CFS Generic Area

Area K Flow

Area A Flow

WWHM2012 PROJECT REPORT

IKP Preserve 0.2 CFS Area

General Model Information

Project Name:

FullDisp .2CFS

Site Name:

Kids Preserve

Site Address:

Johnson Pt Rd

City:

Olympia, WA

Report Date:

3/30/2020

Gage:

Woodard Creek

Data Start:

1955/10/01

Data End:

2011/09/30

Timestep:

15 Minute

Precip Scale:

1.000

Version Date:

2019/09/13

Version:

4.2.17

POC Thresholds

Low Flow Threshold for POC1:

50 Rercent of the 2 Year

High Flow Threshold for POC1:

50 Year

Landuse Basin Data Predeveloped Land Use

| Bear of | | S | | - |
|---------|---|---|-----|---|
| | - | | 110 | - |
| | - | - | | |
| | | | | |

Bypass: No

GroundWater: No

Pervious Land Use acre A B, Forest, Mod 0.13

Pervious Total 0.13

Impervious Land Use acre

Impervious Total 0

Basin Total 0.13

Element Flows To:

Surface Interflow

Groundwater

Mitigated Land Use

Basin 1

Bypass: No

GroundWater: No.

Pervious Land Use acre

Pervious Total 0

Impervious Land Use acre ROADS MOD 0.13

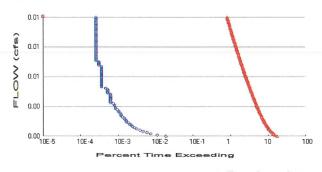
Impervious Total 0.13

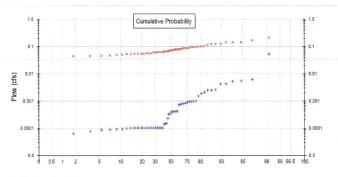
Basin Total 0.13

Element Flows To:

Surface Interflow Groundwater

Analysis Results POC 1





+ Predeveloped

x Mitigated

Predeveloped Landuse Totals for POC #1

Total Pervious Area:

0.13

Total Impervious Area:

0

Mitigated Landuse Totals for POC #1

Total Pervious Area:

0

Total Impervious Area:

0.13

Flow Frequency Method:

Log Pearson Type III 17B

Flow Frequency Return Periods for Predeveloped. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.000344

 5 year
 0.00136

 10 year
 0.003053

 25 year
 0.007767

 50 year
 0.014772

 100 year
 0.027062

Flow Frequency Return Periods for Mitigated. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.073813

 5 year
 0.102245

 10 year
 0.123417

 25 year
 0.152964

 50 year
 0.177091

 100 year
 0.203102

Annual Peaks

Annual Peaks for Predeveloped and Mitigated. POC #1

| Year | Predeveloped | Mitigated |
|------|--------------|-----------|
| 1956 | 0.003 | 0.061 |
| 1957 | 0.000 | 0.098 |
| 1958 | 0.000 | 0.055 |
| 1959 | 0.000 | 0.079 |
| 1960 | 0.001 | 0.145 |
| 1961 | 0.006 | 0.061 |
| 1962 | 0.000 | 0.055 |
| 1963 | 0.003 | 0.117 |
| 1964 | 0.004 | 0.081 |
| 1965 | 0.002 | 0.063 |

Water Quality
Water Quality BMP Flow and Volume for POC #1
On-line facility volume: 0.0326 acre-feet
On-line facility target flow: 0.0427 cfs.
Adjusted for 15 min: 0.0427 cfs.
Off-line facility target flow: 0.0242 cfs.
Adjusted for 15 min: 0.0242 cfs.



Model Default Modifications

Total of 0 changes have been made.

PERLND Changes

No PERLND changes have been made.

IMPLND Changes

No IMPLND changes have been made.



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WWHM2012

PROJECT REPORT

IKP PRESERVE AREA A/B FLOW

General Model Information

Project Name: Area_A-B_Flow

Site Name: IKP Area A/B

Site Address: Johnson Pt Rd

City: Olympia, WA

Report Date: 6/3/2020

Gage: Woodard Creek

Data Start: 1955/10/01 Data End: 2011/09/30

Timestep: 15 Minute

Precip Scale: 1.000

Version Date: 2019/09/13

Version: 4.2.17

POC Thresholds

Low Flow Threshold for POC1: 50 Percent of the 2 Year

High Flow Threshold for POC1: 50 Year

Landuse Basin Data Predeveloped Land Use

Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre SAT, Forest, Mod 0.1613 SAT, Pasture, Steep 0.00403

Pervious Total 0.16533

Impervious Land Use acre ROADS FLAT 0.0023

Impervious Total 0.0023

Basin Total 0.16763

Element Flows To:

Surface Interflow Groundwater

Mitigated Land Use

Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre SAT, Lawn, Mod 0.0545

Pervious Total 0.0545

Impervious Land Use acre
ROADS FLAT 0.0098
ROADS MOD 0.1033

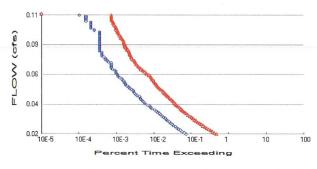
Impervious Total 0.1131

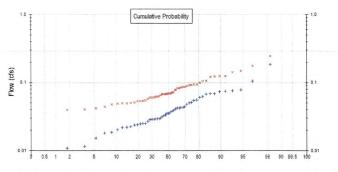
Basin Total 0.1676

Element Flows To:

Surface Interflow Groundwater

Analysis Results POC 1





+ Predeveloped

x Mitigated

Predeveloped Landuse Totals for POC #1

Total Pervious Area: 0.16533 Total Impervious Area: 0.0023

Mitigated Landuse Totals for POC #1
Total Pervious Area: 0.0545
Total Impervious Area: 0.1131

Flow Frequency Method: Log Pearson Type III 17B

Flow Frequency Return Periods for Predeveloped. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.036214

 5 year
 0.058386

 10 year
 0.074139

 25 year
 0.09488

 50 year
 0.110787

 100 year
 0.126993

Flow Frequency Return Periods for Mitigated. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.071009

 5 year
 0.100454

 10 year
 0.122739

 25 year
 0.15425

 50 year
 0.180277

 100 year
 0.208596

Annual Peaks

Annual Peaks for Predeveloped and Mitigated. POC #1

| Year | Predeveloped | Mitigated |
|------|--------------|-----------|
| 1956 | 0.036 | 0.066 |
| 1957 | 0.069 | 0.106 |
| 1958 | 0.029 | 0.055 |
| 1959 | 0.027 | 0.069 |
| 1960 | 0.076 | 0.141 |
| 1961 | 0.029 | 0.060 |
| 1962 | 0.011 | 0.047 |
| 1963 | 0.073 | 0.123 |
| 1964 | 0.060 | 0.089 |
| 1965 | 0.050 | 0.070 |
| | | |

| 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1988 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 2000 2001 2002 2003 2004 2005 2006 2006 2006 2006 2006 | 0.018 0.037 0.024 0.044 0.029 0.030 0.063 0.031 0.029 0.034 0.042 0.043 0.042 0.045 0.043 0.040 0.039 0.022 0.048 0.068 0.015 0.020 0.043 0.068 0.186 0.032 0.025 0.029 0.055 0.105 0.029 0.055 0.0029 0.055 0.0029 0.055 0.0029 0.019 0.025 0.025 | 0.042 0.061 0.054 0.099 0.054 0.058 0.079 0.063 0.085 0.070 0.062 0.083 0.086 0.092 0.072 0.124 0.067 0.068 0.094 0.044 0.086 0.092 0.094 0.044 0.086 0.092 0.075 0.092 0.075 0.093 0.093 0.094 0.093 0.094 0.094 0.095 |
|--|--|---|
| 2005 | 0.019 | 0.039 |

Ranked Annual Peaks

| Natifica / Hillian Leaks | | | |
|--------------------------|-----------------|-------------------------|--------|
| Ranked Annual | Peaks for Prede | eveloped and Mitigated. | POC #1 |
| Rank | Predeveloped | Mitigated | |
| 1 | 0.1855 | 0.2459 | |
| 2 | 0.1051 | 0.1771 | |
| 3 | 0.0781 | 0.1474 | |
| 4 | 0.0757 | 0.1411 | |
| 5 | 0.0743 | 0.1251 | |
| 6 | 0.0733 | 0.1244 | |
| 7 | 0.0689 | 0.1234 | |
| 8 | 0.0683 | 0.1216 | |

| 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 50 51 51 51 51 51 51 51 51 51 51 51 51 51 | 0.0679 0.0625 0.0600 0.0555 0.0546 0.0513 0.0500 0.0479 0.0444 0.0432 0.0431 0.0427 0.0422 0.0419 0.0400 0.0391 0.0359 0.0352 0.0351 0.0352 0.0351 0.0327 0.0327 0.0323 0.0315 0.0302 0.0294 0.0293 0.0293 0.0293 0.0293 0.0293 0.0251 0.0247 0.0247 0.0241 0.0239 0.0252 0.0217 0.0202 0.0187 0.0182 | 0.1067 0.1057 0.0988 0.0941 0.0940 0.0921 0.0916 0.0888 0.0857 0.0856 0.0853 0.0828 0.0793 0.0776 0.0719 0.0719 0.0712 0.0700 0.0698 0.0687 0.0678 0.0678 0.0678 0.0678 0.0656 0.0635 0.0602 0.0602 0.0602 0.0546 0.0543 0.0531 0.0531 0.0548 0.0487 0.0498 0.0493 0.0475 0.0475 |
|---|--|--|
| 50 | 0.0202 | 0.0487 |
| 51 | 0.0187 | 0.0475 |

Model Default Modifications

Total of 0 changes have been made.

PERLND Changes

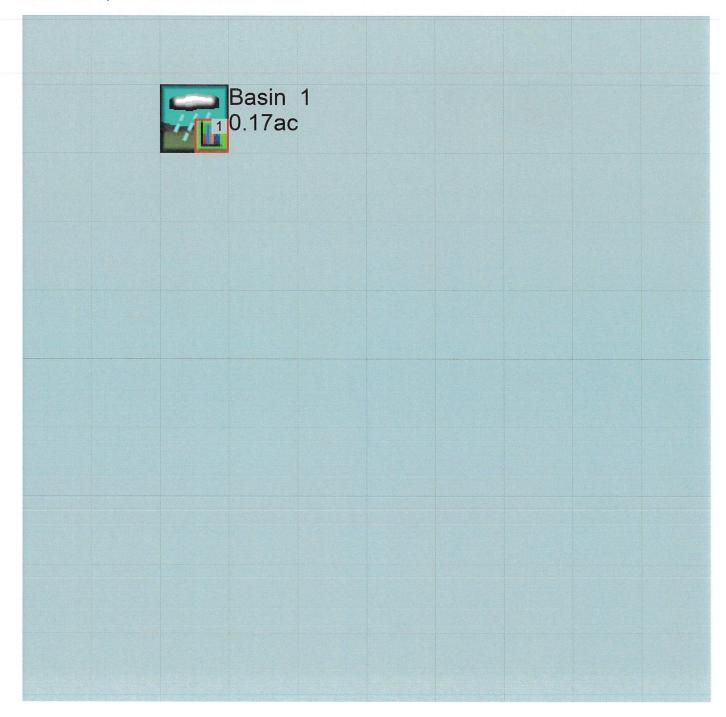
No PERLND changes have been made.

IMPLND Changes

No IMPLND changes have been made.

Area_A-B_Flow 6/3/2020 8:27:29 AM Page 14

Appendix Predeveloped Schematic



Mitigated Schematic



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WWHM2012 PROJECT REPORT

IKP Preserve AREA K FLOW

General Model Information

Project Name: Area_K_Flow

Site Name: IKP

Site Address: Johnson Pt Rd City: Olympia, WA

Report Date: 6/3/2020

Gage: Woodard Creek

 Data Start:
 1955/10/01

 Data End:
 2011/09/30

 Timestep:
 15 Minute

Precip Scale: 1.000

Version Date: 2019/09/13

Version: 4.2.17

POC Thresholds

Low Flow Threshold for POC1: 50 Percent of the 2 Year

High Flow Threshold for POC1: 50 Year

Landuse Basin Data Predeveloped Land Use

Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre C, Forest, Flat 0.1813 SAT, Forest, Flat 0.1813

Pervious Total 0.3626

Impervious Land Use acre

Impervious Total 0

Basin Total 0.3626

Element Flows To:

Surface Interflow Groundwater

Mitigated Land Use

Basin 1

Bypass: No

GroundWater: No

Pervious Land Use acre SAT, Pasture, Flat 0.0717

Pervious Total 0.0717

Impervious Land Use acre ROADS FLAT 0.1096

Impervious Total 0.1096

Basin Total 0.1813

Element Flows To:

Surface Interflow Groundwater Channel 1 Channel 1

Mitigated Routing

Channel 1

Bottom Length: 100.00 ft.
Bottom Width: 4.00 ft.
Manning's n: 0.03
Channel bottom slope 1: 0.02 To 1
Channel Left side slope 0: 3 To 1
Channel right side slope 2: 3 To 1

Infiltration On

Infiltration rate: 0.1 Infiltration safety factor: 1

Wetted surface area On

Total Volume Infiltrated (ac-ft.):

Total Volume Through Riser (ac-ft.):

23.667

Total Volume Through Facility (ac-ft.):

Percent Infiltrated:

Total Precip Applied to Facility:

Total Evap From Facility:

0

Discharge Structure

Riser Height: 0 ft. Riser Diameter: 0 in.

Element Flows To:

Outlet 1 Outlet 2

Channel Hydraulic Table

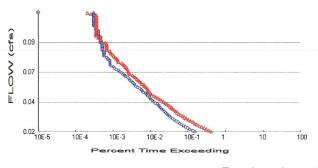
| Stage(feet) | Area(ac.) | Volume(ac-ft.) | Discharge(cfs) | |
|------------------|----------------|----------------|----------------|----------------|
| 0.0000 | 0.009 | 0.000 | 0.000 | 0.000 |
| 0.0111 | 0.009 | 0.000 | 0.015 | 0.000 |
| 0.0222 | 0.009 | 0.000 | 0.049 | 0.001 |
| 0.0333 | 0.009 | 0.000 | 0.097 | 0.001 |
| 0.0444 0.0556 | 0.009 0.009 | 0.000 0.000 | 0.158 0.230 | 0.001 0.001 |
| 0.0667 | 0.010 | 0.000 | 0.230 | 0.001 |
| 0.0007 | 0.010 | 0.000 | 0.405 | 0.001 |
| 0.0889 | 0.010 | 0.000 | 0.507 | 0.001 |
| 0.1000 | 0.010 | 0.001 | 0.619 | 0.001 |
| 0.1111 | 0.010 | 0.001 | 0.740 | 0.001 |
| 0.1222 | 0.010 | 0.001 | 0.870 | 0.001 |
| 0.1333 | 0.011 | 0.001 | 1.008 | 0.001 |
| 0.1444 | 0.011 | 0.001 | 1.156 | 0.001 |
| 0.1556 | 0.011 | 0.001 | 1.312 | 0.001 |
| 0.1667 | 0.011 | 0.001 | 1.476 | 0.001 |
| 0.1778 | 0.011 | 0.001 | 1.649 | 0.001 |
| 0.1889 | 0.011 | 0.002 | 1.830 | 0.001 |
| 0.2000 | 0.011 | 0.002 | 2.019 | 0.001 |
| 0.2111 | 0.012 | 0.002 | 2.217 | 0.001 |
| 0.2222 | 0.012 | 0.002 | 2.423 | 0.001 |
| 0.2333 | 0.012 | 0.002 | 2.636 | 0.001 |
| 0.2444 | 0.012 | 0.002 | 2.858 | 0.001 |
| 0.2556 | 0.012 | 0.002 | 3.088 | 0.001 |
| 0.2667 | 0.012 | 0.002 | 3.326 | 0.001 |
| 0.2778 0.2889 | 0.013 0.013 | 0.003 0.003 | 3.573 3.827 | 0.001 0.001 |
| 0.3000 | 0.013 | 0.003 | 4.089 | 0.001 |
| 0.0000 | 0.013 | 0.005 | ਜ.∪ਹਰ | 0.001 |

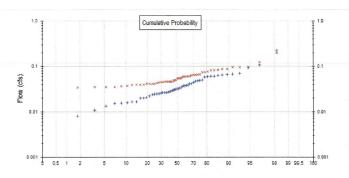
| 0.3111 0.013 0.3222 0.013 0.3333 0.013 0.3444 0.013 0.3556 0.014 0.3667 0.014 0.3778 0.014 0.3889 0.014 0.4000 0.014 0.4111 0.014 0.4222 0.015 0.4333 0.015 0.4444 0.015 0.4556 0.015 0.4778 0.015 0.4889 0.015 0.5000 0.016 0.5111 0.016 0.5333 0.016 0.5444 0.016 0.5556 0.016 0.5544 0.016 0.55444 0.016 0.5556 0.017 0.6000 0.017 0.6111 0.017 0.6333 0.017 0.6444 0.018 0.6556 0.018 0.6778 0.018 0.6778 0.018 0.7778 0.019 0.7789 0.019 <th>0.003 0.003 0.003 0.004 0.004 0.004 0.004 0.004 0.005 0.005 0.005 0.005 0.006 0.006 0.006 0.006 0.006 0.007 0.007 0.007 0.007 0.007 0.008 0.008 0.008 0.008 0.008 0.009 0.009 0.009 0.009 0.010 0.010 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.012 0.012 0.012 0.012 0.012 0.013 0.013 0.013 0.014 0.014 0.014</th> <th>4.359 4.638 4.924 5.219 5.522 6.151 6.479 6.814 7.157 7.509 7.869 8.237 8.614 8.999 9.392 9.793 10.62 11.04 11.48 11.92 12.38 12.84 13.31 14.27 15.79 16.31 16.84 17.38 17.93 18.49 19.63 20.22 21.42 22.03 23.93 24.58 25.91 26.59 27.97 28.60 30.86 31.61 32.37 33.39 33.31 33.31 33.31 33.31</th> <th>0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0</th> | 0.003 0.003 0.003 0.004 0.004 0.004 0.004 0.004 0.005 0.005 0.005 0.005 0.006 0.006 0.006 0.006 0.006 0.007 0.007 0.007 0.007 0.007 0.008 0.008 0.008 0.008 0.008 0.009 0.009 0.009 0.009 0.010 0.010 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.011 0.012 0.012 0.012 0.012 0.012 0.013 0.013 0.013 0.014 0.014 0.014 | 4.359 4.638 4.924 5.219 5.522 6.151 6.479 6.814 7.157 7.509 7.869 8.237 8.614 8.999 9.392 9.793 10.62 11.04 11.48 11.92 12.38 12.84 13.31 14.27 15.79 16.31 16.84 17.38 17.93 18.49 19.63 20.22 21.42 22.03 23.93 24.58 25.91 26.59 27.97 28.60 30.86 31.61 32.37 33.39 33.31 33.31 33.31 33.31 | 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0 |
|---|---|--|--|
|---|---|--|--|

Area_K_Flow 6/3/2020 8:34:22 AM Page 7

| 0.9556 | 0.022 | 0.015 | 34.70 | 0.002 |
|--------|-------|-------|-------|-------|
| 0.9667 | 0.022 | 0.015 | 35.49 | 0.002 |
| 0.9778 | 0.022 | 0.015 | 36.30 | 0.002 |
| 0.9889 | 0.022 | 0.015 | 37.11 | 0.002 |
| 1.0000 | 0.023 | 0.016 | 37.94 | 0.002 |
| 1.0111 | 0.023 | 0.016 | 38.78 | 0.002 |

Analysis Results POC 1





+ Predeveloped

x Mitigated

Predeveloped Landuse Totals for POC #1

Total Pervious Area:

0.3626

Total Impervious Area:

0

Mitigated Landuse Totals for POC #1
Total Pervious Area: 0.0717
Total Impervious Area: 0.1096

Flow Frequency Method: Log Pearson Type III 17B

Flow Frequency Return Periods for Predeveloped. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.032697

 5 year
 0.056234

 10 year
 0.074207

 25 year
 0.09929

 50 year
 0.119541

 100 year
 0.141027

Flow Frequency Return Periods for Mitigated. POC #1

 Return Period
 Flow(cfs)

 2 year
 0.053032

 5 year
 0.07354

 10 year
 0.089141

 25 year
 0.1113

 50 year
 0.129684

 100 year
 0.149764

Annual Peaks

Annual Peaks for Predeveloped and Mitigated. POC #1

| Year | Predeveloped | Mitigated |
|------|--------------|-----------|
| 1956 | 0.037 | 0.049 |
| 1957 | 0.071 | 0.076 |
| 1958 | 0.026 | 0.040 |
| 1959 | 0.024 | 0.046 |
| 1960 | 0.063 | 0.081 |
| 1961 | 0.025 | 0.042 |
| 1962 | 0.008 | 0.037 |
| 1963 | 0.060 | 0.087 |
| 1964 | 0.042 | 0.061 |
| 1965 | 0.047 | 0.054 |

| 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 1999 1999 1999 1999 1999 | 0.016 0.037 0.027 0.030 0.032 0.033 0.066 0.028 0.026 0.022 0.044 0.016 0.034 0.032 0.039 0.049 0.036 0.041 0.030 0.016 0.050 0.058 0.013 0.020 0.061 0.093 0.020 0.026 0.048 0.108 0.017 0.024 0.015 0.024 0.015 0.026 0.038 0.015 | 0.032 0.045 0.034 0.059 0.037 0.041 0.074 0.045 0.046 0.065 0.063 0.066 0.053 0.066 0.046 0.043 0.054 0.074 0.039 0.060 0.066 0.082 0.097 0.046 0.046 0.050 0.097 0.046 0.046 0.050 0.046 0.050 0.065 0.065 0.066 |
|--|---|---|
| 2007 | 0.038 | 0.095 |

Ranked Annual Peaks

Ranked Annual Peaks for Predeveloped and Mitigated. POC #1

Rank

Predeveloped Mitigated

| r ton into or r time on | 1 00110 101 1 1001 | o to lopou a |
|-------------------------|--------------------|--------------|
| Rank | Predeveloped | Mitigated |
| 1 | 0.2248 | 0.1995 |
| 2 | 0.1078 | 0.1246 |
| 3 | 0.0927 | 0.0970 |
| 4 | 0.0710 | 0.0953 |
| 5 | 0.0667 | 0.0940 |
| 6 | 0.0665 | 0.0872 |
| 7 | 0.0645 | 0.0861 |
| 8 | 0.0634 | 0.0834 |

Area_K_Flow 6/3/2020 8:34:53 AM Page 10

| 9 | 0.0612 | 0.0815 |
|----|--------|--------|
| 10 | 0.0607 | 0.0811 |
| 11 | 0.0599 | 0.0759 |
| 12 | 0.0580 | 0.0742 |
| 13 | 0.0501 | 0.0741 |
| 14 | 0.0486 | 0.0659 |
| 15 | 0.0476 | 0.0656 |
| 16 | 0.0470 | 0.0652 |
| 17 | 0.0445 | 0.0651 |
| 18 | 0.0416 | 0.0629 |
| 19 | 0.0414 | 0.0606 |
| 20 | 0.0388 | 0.0601 |
| 21 | 0.0383 | 0.0597 |
| 22 | 0.0368 | 0.0592 |
| 23 | 0.0368 | 0.0588 |
| 24 | 0.0358 | 0.0573 |
| 25 | 0.0337 | 0.0545 |
| 26 | 0.0335 | 0.0541 |
| 27 | 0.0322 | 0.0539 |
| 28 | 0.0318 | 0.0530 |
| 29 | 0.0313 | 0.0499 |
| 30 | 0.0305 | 0.0486 |
| 31 | 0.0300 | 0.0485 |
| 32 | 0.0297 | 0.0461 |
| 33 | 0.0281 | 0.0460 |
| 34 | 0.0281 | 0.0459 |
| 35 | 0.0273 | 0.0458 |
| 36 | 0.0263 | 0.0456 |
| 37 | 0.0263 | 0.0456 |
| 38 | 0.0262 | 0.0448 |
| 39 | 0.0258 | 0.0448 |
| 40 | 0.0250 | 0.0439 |
| 41 | 0.0246 | 0.0430 |
| 42 | 0.0242 | 0.0416 |
| 43 | 0.0240 | 0.0413 |
| 44 | 0.0223 | 0.0412 |
| 45 | 0.0203 | 0.0410 |
| 46 | 0.0200 | 0.0398 |
| 47 | 0.0198 | 0.0398 |
| 48 | 0.0167 | 0.0394 |
| 49 | 0.0165 | 0.0391 |
| 50 | 0.0160 | 0.0371 |
| 51 | 0.0156 | 0.0367 |
| 52 | 0.0152 | 0.0350 |
| 53 | 0.0135 | 0.0346 |
| 54 | 0.0108 | 0.0345 |
| 55 | 0.0080 | 0.0345 |
| 56 | 0.0041 | 0.0345 |

LID Report

| LID Technique | Used for Treatment? | Total Volume Needs Treatment (ac-ft) | Volume Through Facility (ac-ft) | Infiltration Volume (ac-ft) | Cumulative Volume Infiltration Credit | Percent Volume Infiltrated | Water Quality | Percent Water Quality Treated | Comment |
|--|------------------------|---|--|-----------------------------------|--|----------------------------------|---------------|-------------------------------------|--|
| Channel 1 POC | | 22.75 | | | | 5.34 | | | |
| Total Volume Infiltrated | | 22.75 | 0.00 | 0.00 | | 5.34 | 0.00 | 0% | No Treat. Credit |
| Compliance with LID Standard 8% of 2-yr to 50% of 2-yr | | | | | | | | | Duration Analysis Result = Failed |

Model Default Modifications

Total of 0 changes have been made.

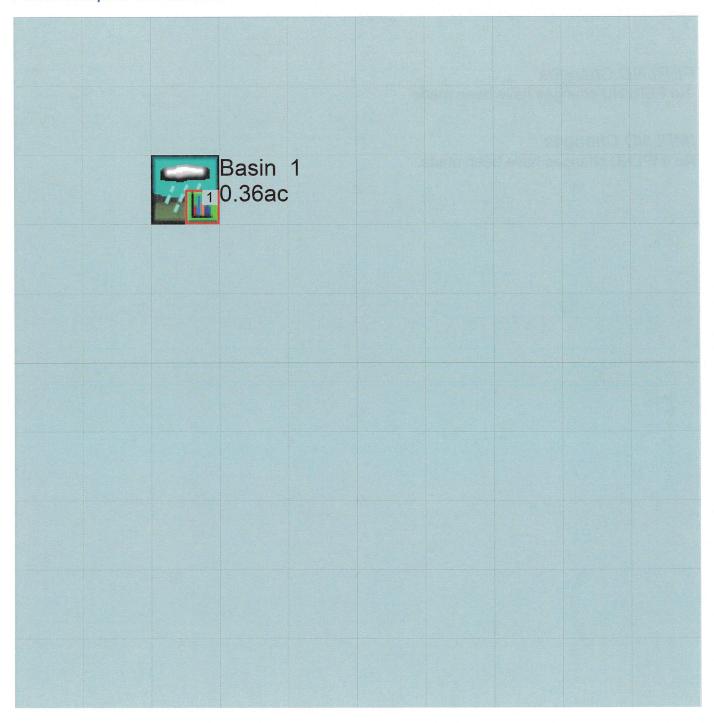
PERLND Changes

No PERLND changes have been made.

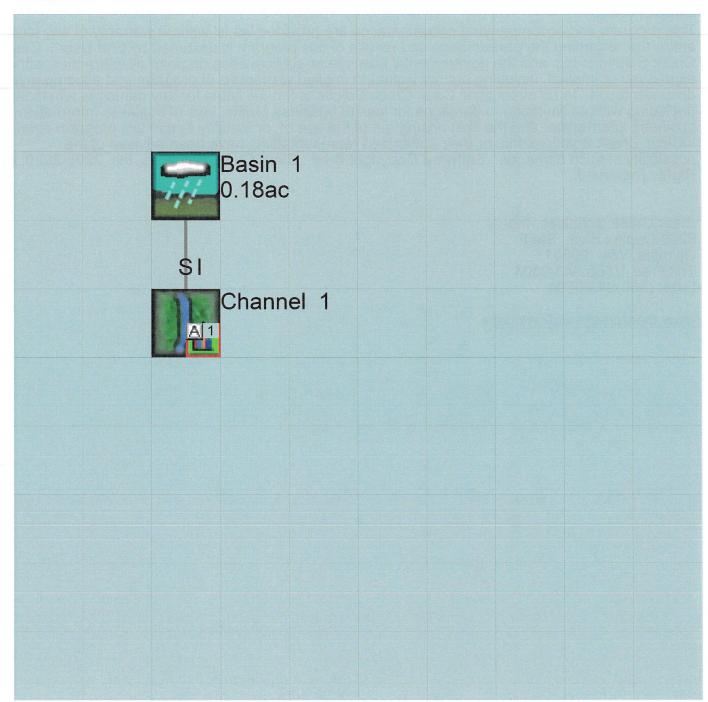
IMPLND Changes

No IMPLND changes have been made.

Appendix Predeveloped Schematic



Mitigated Schematic



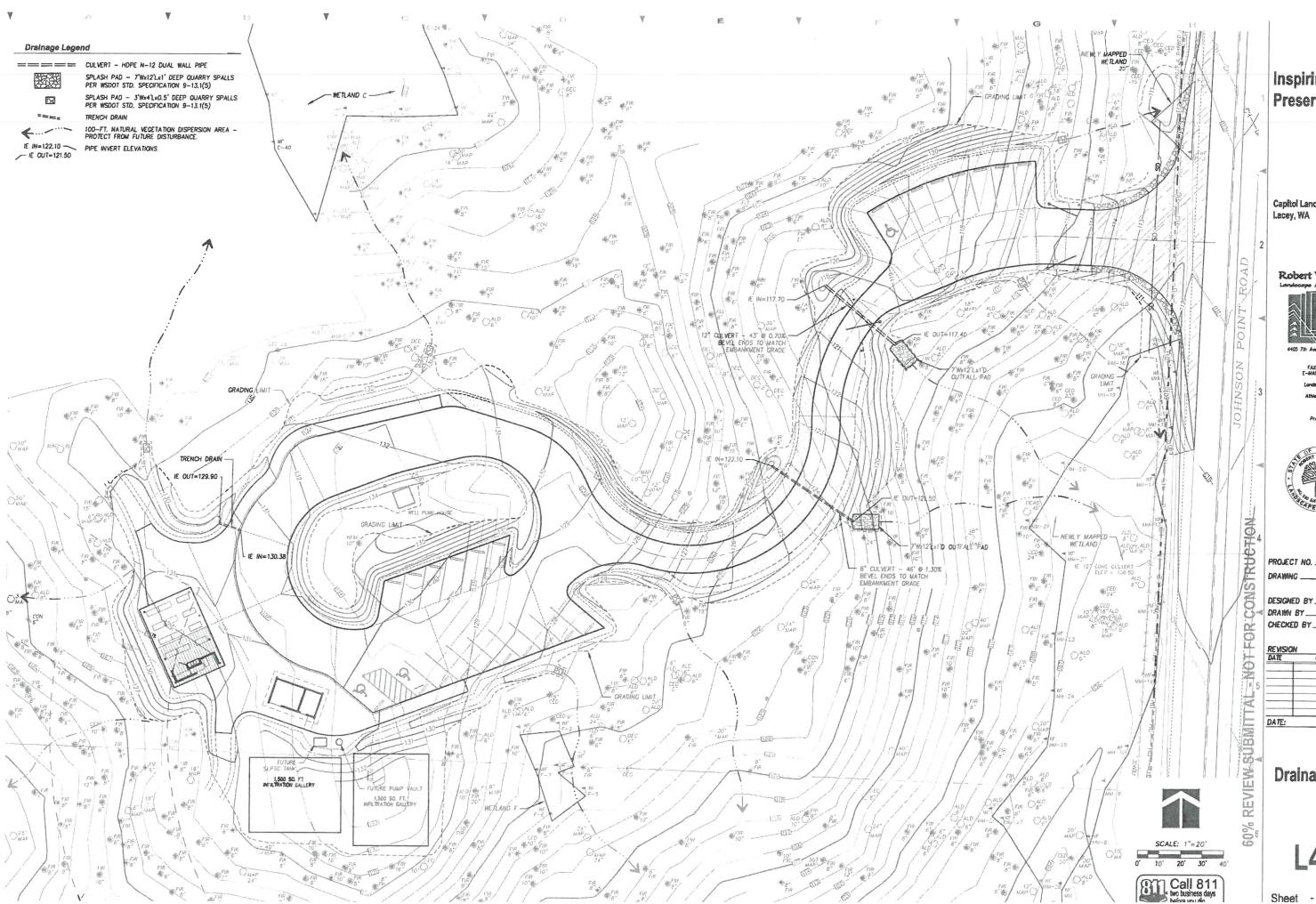
Disclaimer Legal Notice

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www.clearcreeksolutions.com





Inspiring K Preserve

Capitol Land Trust

Robert W. Dr





MAY 22,

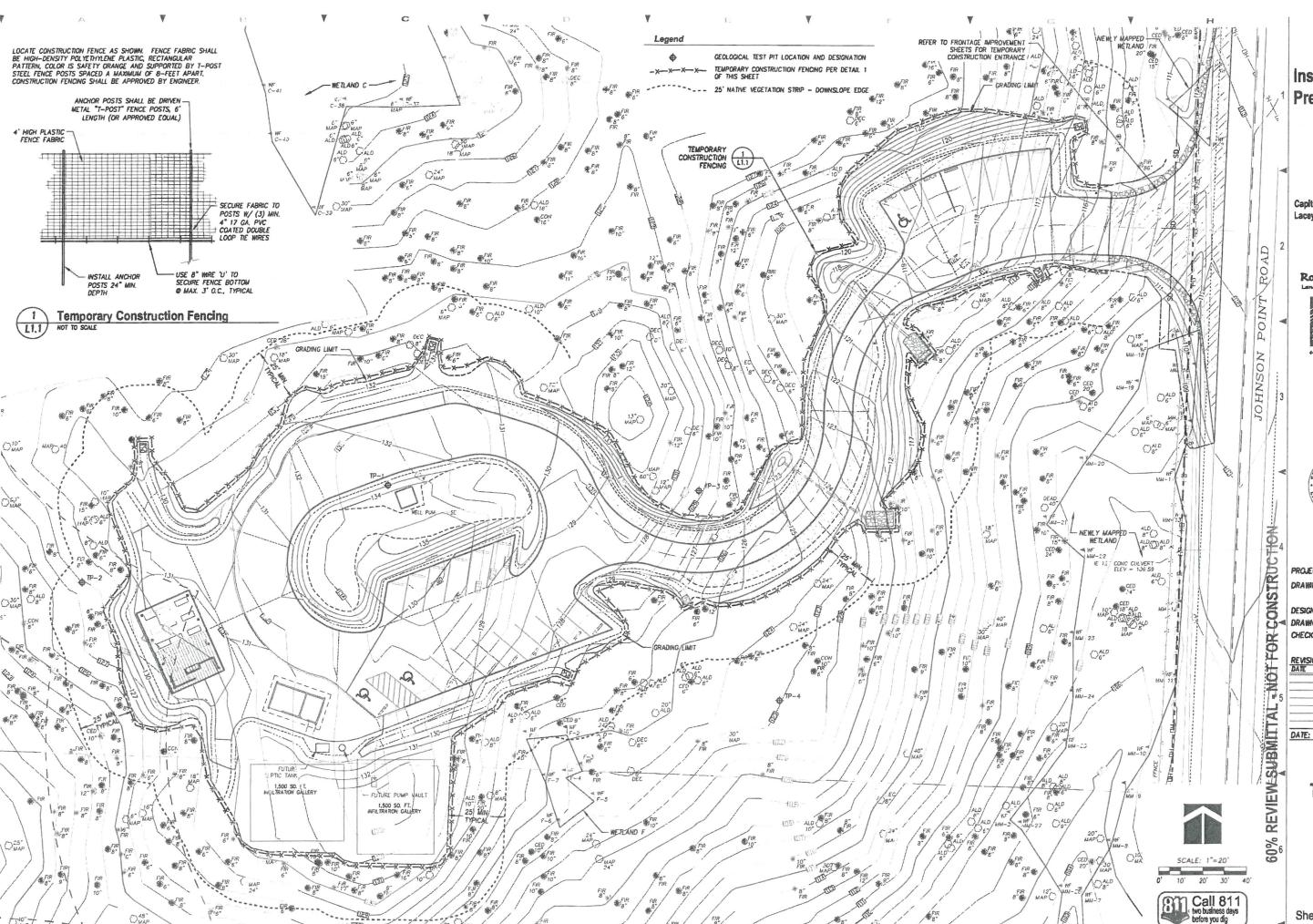
Drainage Pl

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The Construction SWPPP will be prepared and submitted with the final drainage report.



Inspiring K Preserve

Capitol Land Trust Lacey, WA

Robert W. Dr



4405 7th Avenue SE, Ste. Lacey, WA 9 (360) 456-FAX (360) 433-E-MAI bendal

> Londscape Archite Site Ple Athletic Facility Urban



PROJECT NO. _____

DESIGNED BY ______
DRAWN BY _____
CHECKED BY _____

REVISION
DATE CHANGE

TESC Plan

MAY 22,

L1.1

Sheet _-_ of __



The Pollution Source Control Plan will be prepared and submitted with the final drainage report.

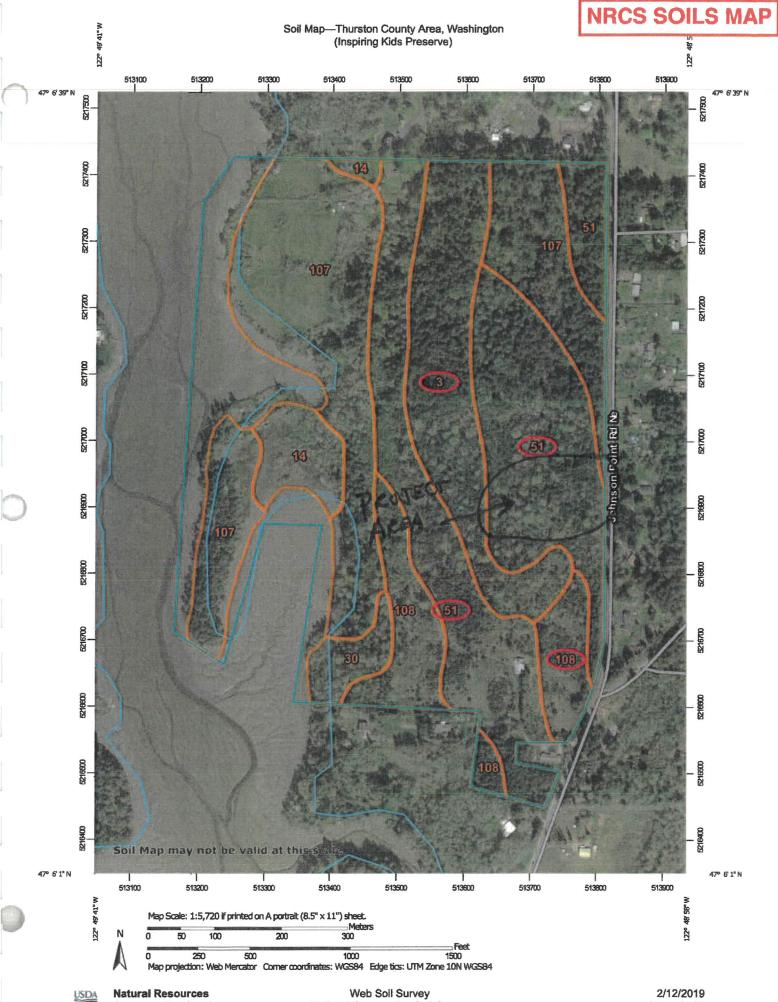
SOURCE CONTROL CHECKLIST

| Activity | | Check if You Are Involved in This | | | |
|-------------|--|--------------------------------------|---------|--|--|
| Code | Type of Activity | Indoor | Outdoor | | |
| <u>A1.1</u> | Cleaning or Washing of Tools, Engines, and Manufacturing Equipment Includes parts washers and all types of manufactured equipment components. | | | | |
| <u>A1.2</u> | Cleaning or Washing of Cooking Equipment Includes vents, filters, pots and pans, grills, and related items. | | | | |
| <u>A1.3</u> | Washing, Pressure Washing, and Steam Cleaning of Vehicles/Equipment/Building Structures Includes cleaning and washing at all types of establishments, including fleet vehicle yards, car dealerships, car washes, and maintenance facilities. | | | | |
| <u>A1.4</u> | Collection and Disposal of Wastewater from Mobile Interior Washing Operations Includes carpet cleaners, upholstery cleaners, and drapery cleaners. | | | | |
| <u>A2.1</u> | Loading and Unloading Areas for Liquid or Solid Material Includes raw materials, intermediate products, finished products, waste, or fuel. | | | | |
| A2.2 | Fueling at Dedicated Stations Includes gas stations, pumps at fleet vehicle yards or shops, and other privately owned pumps. | | | | |
| <u>A2.3</u> | Engine Repair and MaintenanceThis covers oil changes and other engine fluids. | | | | |
| <u>A2.4</u> | Mobile Fueling of Vehicles and Heavy Equipment Includes fleet fueling, wet fueling, and wet hosing. | | | | |
| <u>A3.1</u> | Concrete and Asphalt Mixing and Production at Stationary Sites • Applies to mixing of raw materials on site to produce concrete or asphalt. | | | | |
| <u>A3.2</u> | Concrete Pouring, Concrete Cutting, and Asphalt Application at Temporary Sites Includes construction sites, and driveway and parking lot resurfacing. | | X | | |
| <u>A3.3</u> | Manufacturing and Postprocessing of Metal Products Includes machining, grinding, soldering, cutting, welding, quenching, rinsing, etc. | | | | |
| <u>A3.4</u> | Wood Treatment Areas Includes wood treatment using pressure processes or by dipping or spraying. | | | | |
| <u>A3.5</u> | Commercial Composting • Includes commercial composting facilities operating outside. | | | | |
| <u>A3.6</u> | Landscaping and Vegetation Management Activities, Including Vegetation Removal, Herbicide and Insecticide Application, Fertilizer Application, Irrigation, Watering, Gardening, and Lawn Care Includes businesses involved in landscaping, applying pesticides and managing vegetation. | | X | | |

| Activity | | Check if You Are Involved in This | | |
|--|--|--|--------|--|
| Code | Type of Activity | Indoor | Outdoo | |
| <u>A3.7</u> | Painting, Finishing, and Coating of Vehicles, Boats, Buildings, and Equipment | | | |
| de la companya de la | Includes surface preparation and the applications of paints, finishes, and/or coatings. | | | |
| <u>A3.8</u> | Commercial Printing Operations Includes materials used in the printing process. | | | |
| <u>A3.9</u> | Manufacturing Activities – Outside Includes outdoor manufacturing areas. | | | |
| A3.10 | Agricultural Crop Production Includes commercial scale farming. | | | |
| A3.11 | Application of Pesticides, Herbicides, Fungicides and Rodenticides for purposes other than landscaping Includes moss removal and outdoor insect extermination. | | | |
| <u>A4.1</u> | Storage or Transfer (Outside) of Solid Raw Materials, By-products, or Finished Products | e la companya de la c | | |
| <u>A4.2</u> | Storage and Treatment of Contaminated Soils This applies to contaminated soils that are excavated and left on site. | | | |
| <u>A4.3</u> | Temporary Storage or Processing of Fruits or Vegetables Includes processing activities at wineries, fresh and frozen juice makers, and other food and beverage processing operations. | | | |
| <u>A4.4</u> | Storage of Solid Wastes and Food Wastes Includes regular garbage and all other discarded non-liquid items. | | | |
| <u>A4.5</u> | Recyclers and Scrap Yards Includes scrapped equipment, vehicles, empty metal drums, and assorted recyclables. | | | |
| <u>A4.6</u> | Treatment, Storage, or Disposal of Dangerous Wastes • Refer to Ecology and the Thurston County Health Department for more information, see Chapter 7. | | | |
| <u>A4.7</u> | Storage of Liquid, Food Waste, or Dangerous Waste Containers Includes containers located outside a building and used for temporary storage. | | X | |
| A4.8 | Storage of Liquids in Permanent Aboveground Tanks Includes all liquids in aboveground tanks. | | | |
| <u>A4.9</u> | Parking and Storage for Vehicles and Equipment Includes public and commercial parking lots | | X | |
| <u>A4.10</u> | Storage of Pesticides, Fertilizers, or other products that can leach pollutants | | | |
| <u>A5.1</u> | Demolition of Buildings Applies to removal of existing buildings and subsequent clearing of the rubble. | | X | |
| <u>A5.2</u> | Building Repair, Remodeling, and Construction Applies to construction of buildings, general exterior building repair work and remodeling of buildings. | | X | |

| Activity | | | f You Are d in This | |
|--------------|--|--------|------------------------|--|
| Code | Type of Activity | Indoor | Outdoor | |
| <u>A6.1</u> | Dust Control at Disturbed Land Areas and Unpaved Roadways and Parking Lots | | X | |
| <u>A6.2</u> | Dust Control at Manufacturing Sites Includes grain dust, sawdust, coal, gravel, crushed rock, cement, and boiler fly ash. | | | |
| <u>A6.3</u> | Soil Erosion and Sediment Control (ESC) at Industrial Sites Includes industrial activities that take place on soil. | | | |
| <u>A7.1</u> | Commercial Animal Handling Areas Includes kennels, fenced pens, veterinarians, and businesses that board animals. | | | |
| <u>A7.2</u> | Keeping Livestock in Stables, Pens, Pastures or Fields • Applies to all types of livestock. | | | |
| <u>A7.3</u> | Log Sorting and Handling Applies to log yards typically located at sawmills, ports, and pulp mills. | | | |
| <u>A7.4</u> | Boat Building, Mooring, Maintenance, and Repair Includes all types of maintenance, repair, and building operations. | | | |
| <u>A7.5</u> | Applies to logging activities that fall under Class IV general forest practices. | | | |
| <u>A7.6</u> | Mining and Quarrying of Sand, Gravel, Rock, Minerals, Peat, Clay, and Other Materials This does not include excavation at construction sites. | | | |
| <u>A7.7</u> | Swimming Pool and Spa Cleaning and Maintenance Includes every swimming pool and spa not at a single family residence. Commercial pool cleaners are included here for all pools. | | | |
| <u>A7.8</u> | De-icing and Anti-icing Operations for Airports and Streets • Includes aircraft, runways/taxiways, streets and highways. | | | |
| <u>A7.9</u> | Roof and Building Drains at Manufacturing and Commercial Buildings • These sites will be referred to ORCAA. | | | |
| <u>A7.10</u> | Urban Streets BMPs for addressing pollutants found on paved surfaces, including street sweeping. | | | |
| A7.11 | Railroad Yards | | | |
| <u>A7.12</u> | Maintenance of Public and Private Utility Corridors and Facilities Includes public and private utility maintenance activities. | | | |
| A7.13 | Maintenance of Roadside Ditches | | X | |
| <u>A7.14</u> | Maintenance of Stormwater Drainage and Treatment Facilities | | X | |
| A7.15 | Spills of Oil and Hazardous Substances | | | |

APPENDIX H NRCS Mapping



MAP LEGEND

| Spoil Area | Stony Spot | Very Stony Spot | | wer spor | △ Other | Special Line Features | Water Features | Streams and Canals | Transportation | Rails | Interstate Highways | US Routes | Major Roads | Local Roads | Background | Aerial Photography | | | | |
|------------------------|------------------------|-----------------|------------------------|---------------------|----------------------|------------------------|----------------|--------------------|----------------|-----------|---------------------|------------|---------------|-------------|------------|--------------------|----------------|---------------------|-----------------|--------------|
| | | | | | | | Water | 1 | Trans | ‡ | 3 | K | 2 | | Back | | | | | |
| Area of Interest (AOI) | Area of Interest (AOI) | | Soil Map Unit Polygons | Soil Map Unit Lines | Soil Map Unit Points | Special Point Features | Blowout | Borrow Pit | i | Clay Spot | Closed Depression | Gravel Pit | Gravelly Spot | Landfill | Lava Flow | Marsh or swamp | Mine or Quarry | Miscellaneous Water | Perennial Water | Rock Outcrop |
| Area of In | | Soils | | 1 | | Special | (6) | > | | Ж | \(\) | × | • 8 | 0 | * | 4 | €¢ | 0 | 0 | > |

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at

Warning: Soil Map may not be valid at this scale.

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause line placement. The maps do not show the small areas of scale.

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Thurston County Area, Washington Survey Area Data: Version 12, Sep 10, 2018 Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Apr 1, 2016—Sep 27,

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Severely Eroded Spot

Saline Spot Sandy Spot Slide or Slip

Sinkhole

Sodic Spot

Map Unit Legend

| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|-----------------------------|--|--------------|----------------|
| 3 | Alderwood gravelly sandy loam, 15 to 30 percent slopes | 16.1 | 13.0% |
| 14 | Bellingham silty clay loam | 4.7 | 3.8% |
| 30 | Dystric Xerochrepts, 60 to 90 percent slopes | 2.7 | 2.2% |
| 51 | Kapowsin silt loam, 3 to 15 percent slopes | 38.8 | 31.5% |
| 107 | Skipopa silt loam, 0 to 3 percent slopes | 35.8 | 29.1% |
| 108 | Skipopa silt loam, 3 to 15 percent slopes | 10.5 | 8.5% |
| Totals for Area of Interest | | 123.1 | 100.0% |

Map Unit Description

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions in this report, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named, soils that are similar to the named components, and some minor components that differ in use and management from the major soils.

Most of the soils similar to the major components have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Some minor components, however, have properties and behavior characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. All the soils of a series have major horizons that are similar in composition, thickness, and arrangement. Soils of a given series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A complex consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An undifferentiated group is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Additional information about the map units described in this report is available in other soil reports, which give properties of the soils and the limitations, capabilities, and potentials for many uses. Also, the narratives that accompany the soil reports define some of the properties included in the map unit descriptions.

Report—Map Unit Description

Thurston County Area, Washington

3—Alderwood gravelly sandy loam, 15 to 30 percent slopes

Map Unit Setting

National map unit symbol: 2t627 Elevation: 0 to 1,000 feet



Mean annual precipitation: 25 to 60 inches
Mean annual air temperature: 46 to 52 degrees F

Frost-free period: 160 to 240 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Alderwood and similar soils: 85 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Alderwood

Setting

Landform: Hills, ridges

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Nose slope, side slope, talf

Down-slope shape: Convex, linear Across-slope shape: Convex

Parent material: Glacial drift and/or glacial outwash over dense

glaciomarine deposits

Typical profile

A - 0 to 7 inches: gravelly sandy loam

Bw1 - 7 to 21 inches: very gravelly sandy loam Bw2 - 21 to 30 inches: very gravelly sandy loam Bg - 30 to 35 inches: very gravelly sandy loam 2Cd1 - 35 to 43 inches: very gravelly sandy loam 2Cd2 - 43 to 59 inches: very gravelly sandy loam

Properties and qualities

Slope: 15 to 30 percent

Depth to restrictive feature: 20 to 39 inches to densic material

Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Very

low to moderately low (0.00 to 0.06 in/hr) Depth to water table: About 18 to 37 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4e

Hydrologic Soil Group: B

Forage suitability group: Limited Depth Soils (G002XN302WA), Limited Depth Soils (G002XF303WA), Limited Depth Soils

(G002XS301WA) Hydric soil rating: No

Minor Components

Everett

Percent of map unit: 5 percent



Landform: Moraines, eskers, kames

Landform position (two-dimensional): Backslope Landform position (three-dimensional): Side slope

Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Indianola

Percent of map unit: 5 percent Landform: Kames, eskers, terraces

Landform position (three-dimensional): Tread

Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Shalcar

Percent of map unit: 3 percent

Landform: Depressions

Landform position (three-dimensional): Dip

Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Norma

Percent of map unit: 2 percent

Landform: Drainageways, depressions Landform position (three-dimensional): Dip Down-slope shape: Linear, concave

Across-slope shape: Concave Hydric soil rating: Yes

14—Bellingham silty clay loam

Map Unit Setting

National map unit symbol: 2ndbg

Elevation: 20 to 600 feet

Mean annual precipitation: 25 to 60 inches Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 150 to 200 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Bellingham and similar soils: 85 percent

Minor components: 12 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Bellingham

Setting

Landform: Depressions

Parent material: Alluvium and lacustrine deposits



Typical profile

H1 - 0 to 5 inches: silty clay loam

H2 - 5 to 60 inches: clay

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: More than 80 inches

Natural drainage class: Poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to moderately high (0.06 to 0.20 in/hr)

Depth to water table: About 0 to 12 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: High (about 11.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: C/D

Forage suitability group: Seasonally Wet Soils (G002XN202WA)

Hydric soil rating: Yes

Minor Components

Mckenna

Percent of map unit: 3 percent

Landform: Depressions Hydric soil rating: Yes

Mukilteo

Percent of map unit: 3 percent

Landform: Depressions Hydric soil rating: Yes

Norma

Percent of map unit: 3 percent

Landform: Depressions Hydric soil rating: Yes

Skipopa

Percent of map unit: 3 percent

Hydric soil rating: No

30—Dystric Xerochrepts, 60 to 90 percent slopes

Map Unit Setting

National map unit symbol: 2nd8r

Elevation: 0 to 3,280 feet

Mean annual precipitation: 50 inches Mean annual air temperature: 50 degrees F

Frost-free period: 180 days

Farmland classification: Not prime farmland



Map Unit Composition

Dystric xerochrepts and similar soils: 85 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Dystric Xerochrepts

Setting

Landform: Escarpments

Parent material: Colluvium and glacial till

Typical profile

H1 - 0 to 4 inches: very gravelly sandy loam H2 - 4 to 30 inches: very gravelly sandy loam H3 - 30 to 34 inches: very gravelly sandy loam

Properties and qualities

Slope: 60 to 90 percent

Depth to restrictive feature: 20 to 72 inches to densic material

Natural drainage class: Well drained

Capacity of the most limiting layer to transmit water (Ksat): Very

low to moderately low (0.00 to 0.06 in/hr) Depth to water table: More than 80 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Very low (about 2.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Skipopa

Percent of map unit: 5 percent

Hydric soil rating: No

51—Kapowsin silt loam, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2ndbx

Elevation: 50 to 900 feet

Mean annual precipitation: 30 to 50 inches Mean annual air temperature: 48 to 52 degrees F

Frost-free period: 150 to 220 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Kapowsin and similar soils: 85 percent

Minor components: 8 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Kapowsin

Setting

Landform: Till plains

Parent material: Compact basal till

Typical profile

H1 - 0 to 4 inches: silt loam
H2 - 4 to 22 inches: silt loam
H3 - 22 to 30 inches: gravelly loam
H4 - 30 to 34 inches: gravelly loam

Properties and qualities

Slope: 3 to 15 percent

Depth to restrictive feature: 20 to 40 inches to densic material

Natural drainage class: Moderately well drained

Capacity of the most limiting layer to transmit water (Ksat): Very

low to moderately low (0.00 to 0.06 in/hr) Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Moderate (about 6.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: C/D

Forage suitability group: Limited Depth Soils (G002XN302WA)

Hydric soil rating: No

Minor Components

Norma

Percent of map unit: 5 percent Landform: Depressions Hydric soil rating: Yes

Skipopa

Percent of map unit: 3 percent

Hydric soil rating: No

107—Skipopa silt loam, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2nd7v

Elevation: 490 to 980 feet

Mean annual precipitation: 30 to 50 inches
Mean annual air temperature: 48 to 50 degrees F

Frost-free period: 160 to 200 days

Farmland classification: Prime farmland if drained

Map Unit Composition

Skipopa and similar soils: 85 percent

Minor components: 6 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Skipopa

Setting

Landform: Terraces

Parent material: Volcanic ash over glaciolacustrine deposits

Typical profile

H1 - 0 to 8 inches: silt loam H2 - 8 to 18 inches: silt loam H3 - 18 to 60 inches: clay

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 10 to 20 inches to abrupt textural

change

Natural drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very

low (0.00 in/hr)

Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3w

Hydrologic Soil Group: D

Forage suitability group: Seasonally Wet Soils (G002XN202WA)

Hydric soil rating: No

Minor Components

Bellingham

Percent of map unit: 2 percent

Landform: Depressions Hydric soil rating: Yes

Mukilteo

Percent of map unit: 2 percent

Landform: Depressions Hydric soil rating: Yes

Yelm

Percent of map unit: 2 percent

Hydric soil rating: No

108—Skipopa silt loam, 3 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2nd7w

Elevation: 490 to 980 feet

Mean annual precipitation: 30 to 50 inches Mean annual air temperature: 48 to 50 degrees F

Frost-free period: 160 to 200 days

Farmland classification: Farmland of statewide importance

Map Unit Composition

Skipopa and similar soils: 85 percent

Minor components: 2 percent

Estimates are based on observations, descriptions, and transects of

the mapunit.

Description of Skipopa

Setting

Landform: Terraces

Parent material: Volcanic ash over glaciolacustrine deposits

Typical profile

H1 - 0 to 8 inches: silt loam H2 - 8 to 18 inches: silt loam H3 - 18 to 60 inches: clay

Properties and qualities

Slope: 3 to 15 percent

Depth to restrictive feature: 10 to 20 inches to abrupt textural

change

Natural drainage class: Somewhat poorly drained

Capacity of the most limiting layer to transmit water (Ksat): Very

low (0.00 in/hr)

Depth to water table: About 12 to 24 inches

Frequency of flooding: None Frequency of ponding: None

Available water storage in profile: Low (about 5.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 3e

Hydrologic Soil Group: D

Forage suitability group: Soils with Moderate Limitations

(G002XN602WA) Hydric soil rating: No

Minor Components

Yelm

Percent of map unit: 2 percent



Hydric soil rating: No

Data Source Information

Soil Survey Area: Thurston County Area, Washington

Survey Area Data: Version 12, Sep 10, 2018

File Original and First Copy with Department of Ecology Second Copy—Owner's Copy Third Copy—Driller's Copy

WATER WELL REPORT

ECOLOGY WELL LOG

STATE OF WASHINGTON

| Third Copy—Driller's Copy | Water Right Permit No. |
|--|--|
| (1) OWNER: Name STILLMAN | Address 4844 Johnson PT RD NE |
| (2) LOCATION OF WELL: County THURS TON | NW, SW, Sec 28 T 19N, R/WW. |
| (2a) STREET ADDDRESS OF WELL (or neerest address) | |
| (3) PROPOSED USE: Domestic Industrial Municipal DeWater Test Well Other | Secretion: Describe by color character, size of material and structure, and should |
| _ Derrate. | thickness of aquilers and the kind and nature of the material in each atratum penetrates with all least one entry for each change of information. |
| (4) TYPE OF WORK: (If more than one) | MATERIAL FROM TO |
| Abandoned | do Clay - open role U 29 |
| | chee Clay W/ sand 24 29 |
| Drilled 91 feet. Depth of completed well 86 | n. 5, Hy sand 29 52 |
| (6) CONSTRUCTION DETAILS: | / |
| Casing Installed: Otem. from ft. to Welded Diam. from ft. to | n. Silty sand-scepage 52 60 |
| Liner installed Threeded Diam. from ft. toft. to | " Sand - Fine 60 70 |
| Perforations: Yee No. | Sand- FINE ACTINE 70 86 |
| Type of perforations | in. |
| perforations fromft. to | n Sart W/clay |
| perforations from ft. to | ft. |
| perforations from ft. to | -n v = 8 m |
| Screens: Yes X No | e P |
| Manufacturer's Name | The same of the sa |
| Type WIFE 10 tom B1 1 to B6 | |
| Diam. Sioi esze | |
| Diem. Stot size from ft. to | |
| Gravel packed: Yes No. Siza of gravel | - A |
| Gravel placed from ft. to | |
| Surface seat: Yee No To what depth? | |
| Did any strate contain unuaable water? Yes No | |
| Type of water?Depth of strate | |
| Method of saefing strate off | |
| (7) PUMP: Menufacturer's Name | |
| Type:H.P | |
| (8) WATER LEVELS: Land-surface elevation above maen see level | n. |
| Static level 36 ft. below top of well Cate | |
| Artesian pressure | |
| (Cap, value, exc.)) | Work started Completed 1.1996 |
| (9) WELL TESTS: Drawdown is amount water level is lowered below static | c level |
| Was a pump test made? Vas | WELL CONSTRUCTOR CERTIFICATION: |
| THE STATE OF THE S | constructed and/or accept responsibility for construction of this was |
| 19 II | Materials used and the information reported above are true to my be |
| Recovery data (time taken as zero when pump turned off) (water level maseur | red knowledge and bellef. |
| from well top to water level) Time Water Level Time Water Level Time Water L | NAME TIMS WEW DRULING (PERSON, FIRM, OR CORPORATION) (TYPE/OR PRINT) |
| | - LATTO LIBRO ROLNE |
| + 02 | Address Colf Cibis 9 |
| Date of test | (Signed) The Aug License No. 832 |
| Bailer test gal. / min. with 11. drawdown after | hre. Contractor (WELL DIBLLER) |
| Artest gel./min, with stem set et ft. for | hrs. Registration WO/3/DE Date I- 10 ,199 |
| Artesian flow | R/ |
| Temperature of water Was a chemical energis made? Yes No. | (USE ADDITIONAL SHEETS IF NECESSARY) |



Draft Technical Memorandum

TO: Mr. Bob Droll, President, Robert W. Droll, Landscape Architect, PS

FROM: Lance Levine, PE, and Calvin McCaughan, PE

DATE: March 18, 2020

RE: Summary of Geotechnical Engineering Services

Inspiring Kids Preserve Olympia, Washington

Project No. 1444012.010.011

Introduction

This memorandum summarizes the results of geotechnical engineering services provided by Landau Associates, Inc. (LAI) in support of the Inspiring Kids Preserve project, located at 4849 Johnson Point Road Northeast near Olympia, Washington (site; Figure 1). Geotechnical services were provided in accordance with the scope outlined in LAI's December 6, 2019 proposal.

This memorandum was prepared with information provided by representatives of Robert W. Droll, Landscape Architect, PS, and with data collected during LAI's geologic review, field investigation, and geotechnical laboratory testing. The site plan (Figure 2) was developed with information provided by KPFF Consulting Engineers (project civil engineer).

Project Understanding

The 108-acre site consists of eight undeveloped parcels. Capitol Land Trust (CLT, project owner) proposes to develop a portion of the site along Johnson Point Road Northeast with a shelter, a restroom, trails, paved parking and roads, and one or more stormwater facilities.

Geologic Setting

Geologic information for the site and the surrounding area was obtained from the *Geologic Map of the Lacey 7.5-minute Quadrangle, Thurston County, Washington* (Logan 2003). Subsurface conditions at the site are mapped as Vashon till deposits (Qgt), a highly compact mixture of low-permeability clay, silt, sand, and gravel deposited directly by the glacier. During LAI's February 2020 field investigation, surficial site soils were observed to consist of silt with variable sand content. These soil conditions are consistent with the Vashon recessional outwash and minor silt (Qgos) mapped to the west of the site.

Subsurface Explorations

Site subsurface conditions were explored on February 25, 2020 by excavating five test pits (TP-1 through TP-5) at the approximate locations shown on Figure 2. Howard's Construction and Excavating, subcontracted by LAI, advanced the test pits 12.0 to 15.0 feet (ft) below ground surface (bgs).



LAI personnel monitored the explorations, collected representative soil samples, and maintained a detailed record of the subsurface soil and groundwater conditions observed. Each representative soil type was described using the soil classification system shown on Figure 3. Summary logs of the subsurface soil and groundwater conditions are provided on Figures 4 through 6.

Samples were transported to LAI's soils laboratory for further examination and testing. To evaluate the composition of fine-grained site soils, select samples were analyzed in accordance with ASTM International (ASTM) standard test method D4318, *Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils.* Test results are presented on Figure 7.

Soil Conditions

Soils underlying existing surface conditions (i.e., 6 to 10 inches of topsoil) can be categorized into two units:

- Recessional lacustrine: Recessional lacustrine deposits were observed in all five test pits, and
 consisted of soft, brown or mottled brown silt with variable sand content. The deposits
 exhibited a low bearing capacity and very low infiltration rates.
- **Glacial till:** Glacial till was observed beneath the lacustrine deposits in test pits TP-4 and TP-5. The till varied from dense, brown to gray sand with variable silt and gravel content to very stiff, brown silt.

Cobbles were observed in test pit TP-4, and are often found in glacial till deposits. Cobbles and boulders could be present throughout the site. The contractor should be prepared to manage such oversized material.

Groundwater Conditions

During LAI's February 2020 field investigation, perched groundwater was observed at 6 ft bgs in test pit TP-4. The wetland areas mapped at the site likely store groundwater on top of silt or glacial till layers. A true groundwater table was not observed in LAI's explorations.

The groundwater conditions reported herein are for the specific locations and date indicated, and may not be representative of other locations and/or times. Groundwater conditions will vary with local subsurface conditions, weather conditions, and other factors. Furthermore, groundwater levels are expected to fluctuate seasonally, with maximum groundwater levels occurring during late winter and early spring.

Seismic Design

LAI understands that seismic design will be performed using 2018 International Building Code standards (ICC 2017). The parameters in Table 1 can be used to compute seismic base shear forces.

Table 1. 2018 International Building Code Seismic Design Parameters

| Peak gro | und acceleration = 0.604 |
|------------|--|
| Spectral | response acceleration at short periods $(S_s) = 1.42g$ |
| Spectral | response acceleration at 1-second periods $(S_1) = 0.515g$ |
| Site class | = D |
| Site coef | icient (Fa) = 1.0 |
| Site coef | icient (F _v) = 1.785 ^(a) |

(a) The structural engineer must calculate the seismic response coefficient (C_S) in accordance with Section 11.4.8, Exception 2 of the American Society of Civil Engineers' *Minimum Design Loads and Associated Criteria for Buildings and Other Structures* (2017).

 F_a , F_v = acceleration (0.2-second period) and velocity (1.0-second period) site coefficients, respectively g = force of gravity

 S_s , S_1 = 0.2-second and 1.0-second period spectral accelerations, respectively

Based on the subsurface conditions observed in LAI's February 2020 explorations, seismically induced soil liquefaction and lateral spreading are not likely to occur at the site. Given the distance between the site and the nearest known active crustal fault, the risk of ground rupture due to surface faulting is low.

Conclusions and Recommendations

Shallow site soils are soft, but will provide adequate support for shallow foundations and anticipated structural loads. Because they are fine grained and moisture sensitive, site soils are not suitable for reuse as structural fill. Earthwork should be avoided during heavy and/or extended precipitation events. A 1-ft-thick layer of import structural fill should be placed across structural footprints to limit soil disturbance and increase soil bearing capacity.

Foundation Support

In areas that will be developed with foundations and slabs-on-grade, at least 12 inches of fine-grained, moisture-sensitive soil should be overexcavated and replaced with Gravel Borrow. Gravel Borrow should meet the requirements in Section 9-03.14(1) of the Washington State Department of Transportation's 2020 Standard Specifications for Road, Bridge, and Municipal Construction (2020 WSDOT Standard Specifications). Following overexcavation, the exposed subgrade should be sloped to allow runoff to drain away from the proposed structures. Gravel Borrow should be compacted to 95 percent of the maximum dry density, in accordance with ASTM standard test method D1557, Standard Test Methods for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft³ (2,700 kN-m/m³)).

The design parameters in Table 2 should be used in conjunction with the complete recommendations in this memorandum.

Table 2. Summary of Design Parameters for Shallow Foundations

Allowable soil bearing pressure = 2,000 psf

Friction coefficient (factored) = 0.35

Passive earth pressure = 250 pcf

Minimum foundation width = 18 inches (continuous), 24 inches (isolated)

Maximum foundation width (for settlement considerations) = 5 ft (continuous), 10 ft (isolated)

ft = feet pcf = pounds per cubic foot psf = pounds per square foot

When calculating design parameters, LAI assumed that shallow foundations would be constructed on 1 ft of Gravel Borrow extending to uniformly firm, unyielding, unsaturated silt. The allowable soil bearing pressure in Table 2 applies to long-term dead and live loads, exclusive of the weight of the footing and any overlying backfill. The allowable soil bearing pressure includes a factor of safety of at least 3 on the calculated ultimate bearing capacity. The allowable soil bearing pressure can be increased by one-third for total loads, including transient loads, such as those induced by wind and seismic forces.

LAI recommends a minimum width of 18 inches for continuous wall footings and 24 inches for isolated column footings. For frost protection, perimeter footings should be embedded at least 12 inches below the lowest adjacent grade, where the ground is flat. If used, interior footings should be embedded at least 6 inches below the nearest adjacent grade. If construction is performed as recommended, settlement of continuous or isolated foundations is estimated to be on the order of 1 inch or less. Differential settlement between similarly loaded foundation elements is estimated to be on the order of ½ inch or less. Settlement is likely to occur as building loads are applied during construction.

An allowable coefficient of sliding resistance of 0.35, applied to vertical dead loads only, can be used to compute frictional resistance acting on the base of footings. The allowable coefficient of sliding resistance includes a factor of safety of 1.5 on the calculated ultimate value.

The passive resistance of properly compacted structural fill placed against the sides of foundations can be considered equivalent to a fluid with a density of 250 pounds per cubic foot (pcf). The foundation passive earth pressure value has been reduced by a factor of 1.5 to limit deflections to less than 2 percent of the embedded depth. The passive earth pressure and friction components can be combined, provided the passive component does not exceed two-thirds of the total. The top foot of soil should be excluded from the calculation, unless the foundation perimeter will be covered by a slab-on-grade or pavement.

Slabs-On-Grade

A modulus of vertical subgrade reaction (subgrade modulus) can be used to design slabs-on-grade. The subgrade modulus will vary based on the dimensions of the slab and the magnitude of applied loads on the slab surface; slabs with larger dimensions and loads are influenced by soils at a greater depth. LAI recommends using a subgrade modulus of 125 pounds per cubic inch to design on-grade floor slabs. This subgrade modulus is for a 1-ft by 1-ft square plate, and is not the overall modulus of a larger area. When calculating the subgrade modulus, LAI assumed that on-grade slabs would be placed on a 1-ft-thick layer of Gravel Borrow.

Interior slabs-on-grade should include a vapor barrier and a capillary break layer, consistent with industry standards. The 1-ft-thick layer of Gravel Borrow placed beneath slabs to limit subgrade disturbance could double as a capillary break material, provided it is not contaminated with silty soils during construction.

Pavement Design

Pavement sections should be constructed on a uniformly firm, unyielding subgrade that consists of 1 ft of recompacted native soil or import structural fill. Native soils will not provide a suitable subbase for pavements constructed during the wet season. If wet weather construction is unavoidable, one foot of import structural fill should be placed beneath the pavement section.

When calculating the parameters in Table 3, LAI assumed a 20-year design life and maximum equivalent single-axle loads of 100,000 for the standard-duty pavement section and 1,000,000 for the heavy-duty section. For new pavement installed within public rights-of-way, local standards will supersede the recommendations provided herein.

Table 3. Recommended Asphalt Pavement Design Section

| Pavement Section Type | Asphalt Pavement Thickness (inches) | Crushed Surfacing Thickness (inches) | | |
|-----------------------|---|--------------------------------------|--|--|
| Standard duty | 2 | 4 | | |
| Heavy duty | 3 | 6 | | |

Base course material should be compacted to at least 95 percent of the maximum dry density (ASTM standard test method D1557), and should meet the requirements for Crushed Surfacing Base Course in Section 9-03.9(3) of the 2020 WSDOT Standard Specifications. To facilitate fine grading of the surface, the upper 2 inches of crushed surfacing could consist of Crushed Surfacing Top Course. Prevention of road base saturation is essential for pavement durability, and efforts should be made to limit the amount of water entering the base course.

Asphalt concrete should be Class B aggregate material or hot-mix asphalt class ½ inch and PG58H-22 binder conforming to the requirements in Section 5-04 of the 2020 WSDOT Standard Specifications. Asphalt should be compacted to at least 91 percent of the Rice density.

Stormwater Infiltration

The site is underlain by silt with variable sand content and by impermeable glacial till. These soils have a low infiltration rate, and wetlands have formed in areas of the site with water ponding. Based on the subsurface conditions observed in LAI's February 2020 explorations, onsite stormwater infiltration may not be feasible. Fine-grained site soils are likely to have a limited infiltration rate of 0.05 inches per hour.

Site Work

The following key points should be reviewed during development of design specifications:

- Stripping: Organic-rich topsoil is present throughout the site, and extends approximately 1 ft
 bgs. LAI recommends stripping the sod/topsoil from beneath all structural areas (i.e., footings,
 slabs-on-grade, and pavement sections). An average stripping depth of 1 ft should be
 assumed. Stripped material is not suitable for reuse as structural fill, but can be stockpiled and
 used in landscaped areas.
- Subgrade preparation: Before structural fill or formwork is placed, the subgrade should be
 evaluated by the geotechnical engineer. Accessible subgrades should be proof-rolled; areas of
 limited access can be evaluated using a steel T-probe. If probing or proof-rolling reveals loose
 and/or disturbed subgrades, the upper 1 ft of subgrade should be scarified, moisture
 conditioned, and compacted to a firm, unyielding condition, or overexcavated and replaced
 with compacted structural fill.
- Site utilities: Site soils are anticipated to provide adequate foundation support for new utility
 lines. Unsuitable soil should be overexcavated and replaced with crushed, processed, or
 naturally occurring granular material. The material should meet the gradation requirements
 for Gravel Backfill for Pipe Zone Bedding in Section 9-03.12(3) of the 2020 WSDOT Standard
 Specifications. Foundation material should be placed in 6-inch lifts and mechanically
 compacted to provide a firm trench bottom.
- Site soils: Nearly all site soils are fine grained and moisture sensitive. Earthwork should be
 avoided during heavy and/or extended precipitation events. Native soils will require moisture
 conditioning, even in dry summer months. If reused as structural fill, native soils should be
 moisture conditioned and screened for constituents greater than 6 inches in diameter. In LAI's
 opinion, large-scale reuse of native soils is impractical, as preparation could delay the project
 schedule.
- Import structural fill: Gravel Borrow, as described in Section 9-03.14(1) of the 2020 WSDOT Standard Specifications, is a suitable source of import structural fill. During periods of wet weather, the fines content should not exceed 5 percent, based on the minus ¾-inch fraction.

- **Fill placement and compaction:** Structural fill should be placed on an approved subgrade that consists of uniformly firm, unyielding, inorganic native soil, or on compacted structural fill extending to such soils. Structural fill should be placed and compacted in accordance with Section 2-03.3(14)C, Method C of the *2020 WSDOT Standard Specifications*. Method A is appropriate for non-structural areas, such as landscaping. Each layer of structural fill should be compacted to at least 95 percent of the maximum dry density, as determined using the compaction control tests described in Section 2-03.3(14)D of the *2020 WSDOT Standard Specifications*. Alternatively, maximum density can be determined using ASTM standard test method D1557.
- Construction dewatering: Perched groundwater zones may be encountered during the wet season, and the need for construction dewatering should be anticipated. LAI recommends dewatering temporary excavations to allow construction to be completed in the dry. Where groundwater seepage is encountered, conventional sumps and pumps should be sufficient. The contractor should be responsible for the design, monitoring, and maintenance of any dewatering system(s).
- Temporary slopes: Temporary excavations should be completed in accordance with Section 2-09 of the 2020 WSDOT Standard Specifications. The contractor should be responsible for actual excavation configurations and the maintenance of safe working conditions, including temporary excavation stability. Temporary excavations in excess of 4 ft should be shored or sloped in accordance with the requirements outlined in Safety Standards for Construction Work, Part N (Washington Administrative Code Chapter 296-155). The soil likely to be exposed in the excavations should be considered Type C with a maximum allowable excavation inclination of 1½ horizontal to 1 vertical (1½H:1V). All applicable local, state, and federal safety codes should be followed.
- Permanent slopes: Permanent cut-or-fill slopes should be no steeper than 2H:1V. This design
 recommendation does not apply to stormwater pond slopes, which are typically 3H:1V or
 flatter. Stormwater pond slopes should be designed in accordance with local stormwater
 codes. Permanent and temporary slopes should be protected from erosion and reseeded or
 revegetated as soon as practical.
- Obstructions: During LAI's February 2020 field investigation, cobbles were observed in site soils. The contractor should be prepared to encounter cobbles and boulders in the excavations.

Construction Support Services

LAI should review the project plans and specifications to verify that geotechnical recommendations have been properly interpreted and implemented.

Monitoring, testing, and consultation should be provided during construction to confirm that site conditions are consistent with those observed in LAI's explorations, and to provide expedient recommendations should conditions differ from those anticipated. Construction monitoring activities would include compaction testing of structural fill and observation of slab, pavement, and structural foundation subgrade preparation. LAI would be pleased to provide construction monitoring services.

Use of This Technical Memorandum

Landau Associates, Inc. (LAI) has prepared this technical memorandum for the exclusive use of Capitol Land Trust; Robert W. Droll, Landscape Architect, PS; and the project design team for specific application to the Inspiring Kids Preserve project in Olympia, Washington. No other party is entitled to rely on the information, conclusions, and recommendations included in this document without the express written consent of LAI. Reuse of the information, conclusions, and recommendations provided herein for extensions of the project or for any other project, without review and authorization by LAI, shall be at the user's sole risk. LAI warrants that, within the limitations of scope, schedule, and budget, its services have been provided in a manner consistent with that level of skill and care ordinarily exercised by members of the profession currently practicing in the same locality under similar conditions as this project. LAI makes no other warranty, either express or implied.

Closing

We trust that this memorandum provides you with sufficient information to proceed with the project. If you have questions or comments, please contact the undersigned at (360) 791-3178.

LANDAU ASSOCIATES, INC.

Lance Levine, PE Senior Project Engineer

Calvin McCaughan, PE Principal

LGL/CAM/mcs

[O:\1444\012.010\R\INSPIRING KIDS PRESERVE DRAFT TECHNICAL MEMORANDUM 3.18.2020.DOCX]

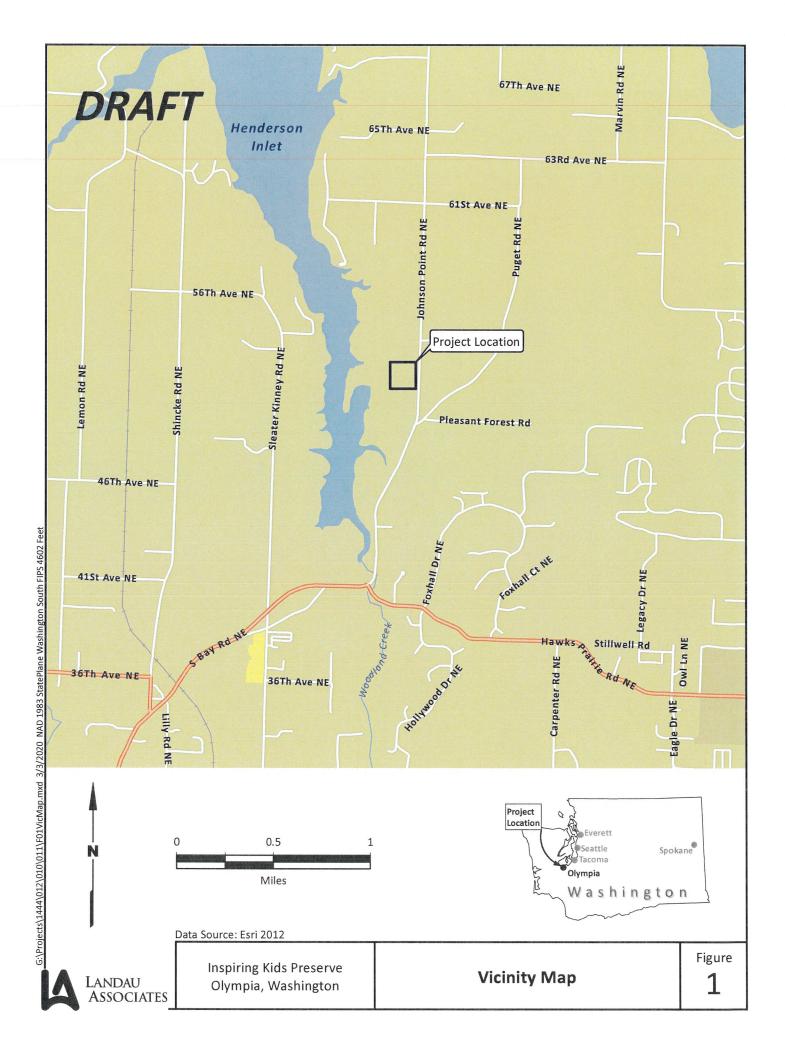
Attachments: Figure 1. Vicinity Map

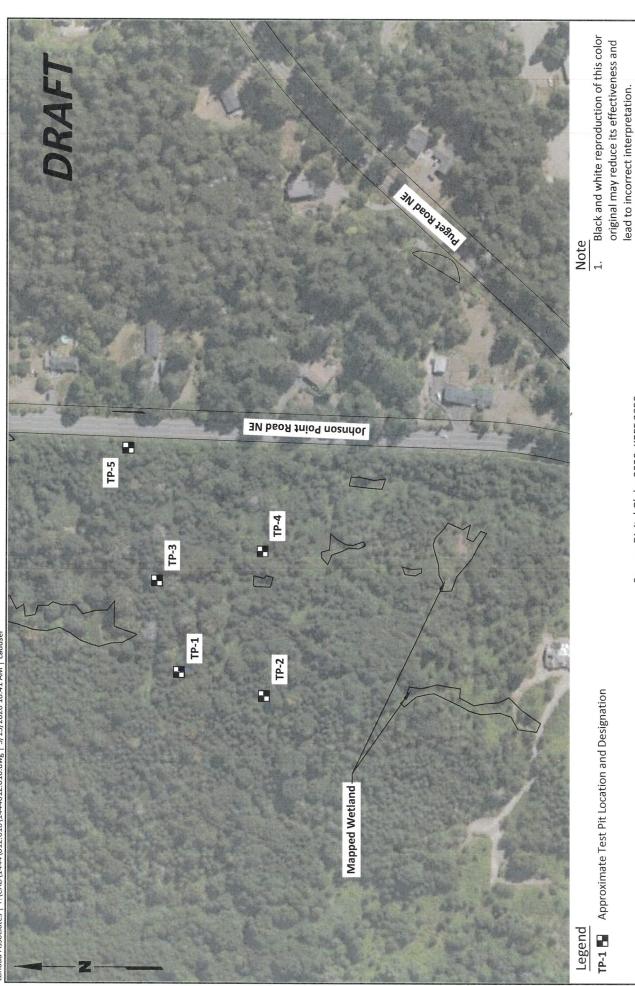
Figure 2. Site and Exploration Location Plan Figure 3. Soil Classification System and Key

Figures 4–6. Logs of Test Pits Figure 7. Plasticity Chart

References

- ASCE. 2017. Minimum Design Loads and Associated Criteria for Buildings and Other Structures (ASCE/SEI 7-16). American Society of Civil Engineers/Structural Engineering Institute.
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- Washington State Department of Labor and Industries. 2016. Construction Work. Chapter 296-155 WAC; Part N. Excavation, Trenching, and Shoring. Washington State Department of Labor and Industries. May 20.
- WSDOT. 2019. *M41-10: Standard Specifications for Road, Bridge, and Municipal Construction 2020.*Washington State Department of Transportation.





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Source: Digital Globe 2020; KPFF 2020

Inspiring Kids Preserve Olympia, Washington

400

200

Site and Exploration Location Plan

Figure

LANDAU
ASSOCIATES

Scale in Feet

Soil Classification System

| | MAJOR DIVISIONS | | | USCS LETTER SYMBOL ⁽¹⁾ | TYPICAL DESCRIPTIONS (2)(3) | | |
|--|--|--|--|---|---|--|--|
| SOIL rial is size) | GRAVEL AND GRAVELLY SOIL | CLEAN GRAVEL (Little or no fines) | | GW GP | Well-graded gravel; gravel/sand mixture(s); little or no fines Poorly graded gravel; gravel/sand mixture(s); little or no fines | | |
| ED mate sieve | (More than 50% of coarse fraction retained on No. 4 sieve) | GRAVEL WITH FINES (Appreciable amount of | | GM | Silty gravel; gravel/sand/silt mixture(s) | | |
| COARSE-GRAINED (More than 50% of mate larger than No. 200 siev | SAND AND SANDY SOIL | fines) CLEAN SAND (Little or no fines) | チスクイン | GC SW | Clayey gravel; gravel/sand/clay mixture(s) Well-graded sand; gravelly sand; little or no fines | | |
| | (More than 50% of coarse fraction passed | SAND WITH FINES | | SP SM | Poorly graded sand; gravelly sand; little or no fines Silty sand; sand/silt mixture(s) | | |
| | through No. 4 sieve) | (Appreciable amount of fines) | | SC | Clayey sand; sand/clay mixture(s) | | |
| INE-GRAINED SOIL (More than 50% of material is smaller than No. 200 sieve size) | | ND CLAY | | ML CL | Inorganic silt and very fine sand; rock flour; silty or clayey fine sand or clayey silt with slight plasticity Inorganic clay of low to medium plasticity; gravelly clay; sandy clay; silty clay; lean clay | | |
| | (Liquid limi | t less than 50) | | OL | Organic silt; organic, silty clay of low plasticity | | |
| | SILT A | ND CLAY | | MH | Inorganic silt; micaceous or diatomaceous fine sand Inorganic clay of high plasticity; fat clay | | |
| FINE mate No | (Liquid limit | greater than 50) | | ОН | Organic clay of medium to high plasticity; organic silt | | |
| | | | \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | | | | |

| OTHER MATERIALS | GRAPHIC LETTER SYMBOL | TYPICAL DESCRIPTIONS |
|-----------------|-----------------------|---|
| PAVEMENT | AC or PC | Asphalt concrete pavement or Portland cement pavement |
| ROCK | RK | Rock (See Rock Classification) |
| WOOD | WD | Wood, lumber, wood chips |
| DEBRIS | 6/6/6/ DB | Construction debris, garbage |

- Notes: 1. USCS letter symbols correspond to symbols used by the Unified Soil Classification System and ASTM classification methods. Dual letter symbols (e.g., SP-SM for sand or gravel) indicate soil with an estimated 5-15% fines. Multiple letter symbols (e.g., ML/CL) indicate borderline or multiple soil classifications.
 - Soil descriptions are based on the general approach presented in the Standard Practice for Description and Identification of Soils (Visual-Manual Procedure), outlined in ASTM D 2488. Where laboratory index testing has been conducted, soil classifications are based on the Standard Test Method for Classification of Soils for Engineering Purposes, as outlined in ASTM D 2487.
 - 3. Soil description terminology is based on visual estimates (in the absence of laboratory test data) of the percentages of each soil type and is defined as follows:

Primary Constituent:
> 50% - "GRAVEL," "SAND," "SILT," "CLAY," etc.

Secondary Constituents:
> 30% and \(\leq 50\)% - "very gravelly," "very sandy," "very silty," etc.

> 15% and \(\leq 30\)% - "gravelly," "sandy," "silty," etc.

Additional Constituents:
> 5% and \(\leq 15\)% - "with gravel," "with sand," "with silt," etc.

\(\leq 5\)% - "with trace gravel," "with trace sand," "with trace silt," etc., or not noted.

4. Soil density or consistency descriptions are based on judgement using a combination of sampler penetration blow counts, drilling or excavating conditions, field tests, and laboratory tests, as appropriate.

| | Drilling and Sam | Fie | Field and Lab Test Data | | | |
|------------------------|---|--|---|--|--|--|
| | SAMPLER TYPE | SAMPLE NUMBER & INTERVAL | | | | |
| Code a b c d e f g h i | Description 3.25-inch O.D., 2.42-inch I.D. Split Spoon 2.00-inch O.D., 1.50-inch I.D. Split Spoon Shelby Tube Grab Sample Single-Tube Core Barrel Double-Tube Core Barrel 2.50-inch O.D., 2.00-inch I.D. WSDOT 3.00-inch O.D., 2.375-inch I.D. Mod. California Other - See text if applicable 300-lb Hammer, 30-inch Drop | Sample Identification Number Recovery Depth Interval Sample Depth Interval Portion of Sample Retained for Archive or Analysis | Code PP = 1.0 TV = 0.5 PID = 100 W = 10 D = 120 -200 = 60 GS AL GT CA | Description Pocket Penetrometer, tsf Torvane, tsf Photoionization Detector VOC screening, ppm Moisture Content, % Dry Density, pcf Material smaller than No. 200 sieve, % Grain Size - See separate figure for data Atterberg Limits - See separate figure for data Other Geotechnical Testing Chemical Analysis | | |
| 2 | 140-lb Hammer, 30-inch Drop Pushed | Groundwater | | | | |
| 4 5 | Vibrocore (Rotosonic/Geoprobe) Other - See text if applicable | Approximate water level at time of control Approximate water level at time after | 0 , , | tion/well | | |



Inspiring Kids Preserve Olympia, Washington

HIGHLY ORGANIC SOIL

Soil Classification System and Key

Peat; humus; swamp soil with high organic content

| SAMPLE DATA | SOIL PROFILE | GROUNDWATER |
|--|---|------------------------------|
| Elevation (ft) Sample Number & Interval Sampler Type | Excavation Method: Tracked Excavator Ground Elevation (ft): Not measured Excavated By: Howard's Construction and Excav. Logged By: DAR 3 inches of duff over 7 inches of dark brown SILT with sand and organics (soft, moist) (TOPSOIL) Brown SILT with sand (soft, moist) (RECESSIONAL LACUSTRINE) | Groundwater not encountered. |

TP-2

| SAMPLE DATA | | | | | | | SOIL PROFILE | GROUNDWATER |
|--------------------------------|----------------|-----------------------------|--------------|--------------------------------|----------------|-------------|--|------------------------------|
| o Depth (ft) | Elevation (ft) | Sample Number & Interval | Sampler Type | Test Data | Graphic Symbol | USCS Symbol | Excavation Method: Tracked Excavator Ground Elevation (ft): Not measured Excavated By: Howard's Construction and Excav. Logged By: DAR | |
| 0 5 | | S-1 | d | W = 37 AL | | ML ML | 3 inches of duff over 6 inches of dark brown SILT with sand and organics (soft, moist) (TOPSOIL) Mottled orange/brown/gray SILT with sand (soft, moist to wet) (RECESSIONAL LACUSTRINE) | Groundwater not encountered. |
| - 10 | 2 2 | S-2 | d | | | SM | Brown, very silty, fine SAND (medium dense, moist) | |
| | T | | | ted 02/25/20 Pit = 12.0 ft. | | | | |

Notes:

Stratigraphic contacts are based on field interpretations and are approximate.
 Reference to the text of this report is necessary for a proper understanding of subsurface conditions.
 Refer to "Soil Classification System and Key" figure for explanation of graphics and symbols.



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1444012.010.011 3/10/20 \\OLYMPIA1\PROJECTS\1444\012.010\\T\1444012.010.GPJ TEST PIT LOG W/ ELEVATION

20

Inspiring Kids Preserve Olympia, Washington

Log of Test Pits

Figure

| | SA | MPLE D | ATA | 1 | | | SOIL | | GROUNDWA | TER | |
|---|----------------|--|--------------------|---|----------------|----------------------------------|---|---|----------|-------------------------------|-------|
| | | per | e e | | loqu | 0 | Excavation Metho | od: Tracked Excavator | | | |
| | Elevation (ft) | N L | Sampler Type | ā | Graphic Symbol | Symbol | Ground Elevation | | | | |
| | atio | ple | pler | Test Data | ohic | SS | Excavated By: _ | Howard's Construction and Ex | xcav. | | |
| | Elev | Sample Number & Interval | San | Test | Gray | nscs | Logged By: | DAR | | | |
|) | | | | | Ш | ML | | ver 7 inches of dark brown and organics (soft, moist) | | | |
| | | S-1 | d | W = 33 AL | Ш | ML | SILT WILL SALID A | (TOPSOIL) | | Groundwater not encounted | ered. |
| 5 | | | | | | | Brown SILT with (RECESS | sand (soft, moist) SIONAL LACUSTRINE) | | | |
| | | S-2 | d | | | SM | Brown, very silty, | fine SAND (loose, moist) | | | |
| 0 | | | | | H | ML | Brown SILT (soft, | moist) | | | |
| | | S-3 Test Pit (| d | eted 02/25/20 | Ш | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | P-4 | | | |
| | SA | MPLE [| DATA | \ | | | | PROFILE | | GROUNDWA | TER |
| | | | | A | loqui | lodi | SOIL I | PROFILE od: Tracked Excavator | | GROUNDWA | TER |
| | | | | | c Symbol | Symbol | SOIL I | PROFILE Od: Tracked Excavator (ft): Not measured | | GROUNDWA | TER |
| | | | | | aphic Symbol | SCS Symbol | Excavation Methor Ground Elevation Excavated By: | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Ex | xcav. | GROUNDWA | TER |
| | Elevation (ft) | Sample Number 3 3 3 8 Interval | Sampler Type | Test Data | Graphic Symbol | I USCS Symbol | Excavation Methor Ground Elevation Excavated By: Logged By: | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Excavator | xcav. | GROUNDWA | TER |
| | | Sample Number & Interval | Sampler Type | Es = A | Graphic Symbol | NSCS Symbol | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of | PROFILE Od: Tracked Excavator (ft): Not measured Howard's Construction and Excavator OAR over 7 inches of dark brown and organics (soft, moist) | xcav. | GROUNDWA | TER |
| | | Sample Number & Interval | a Sampler Type | Test Data | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand and | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Excavator OAR ver 7 inches of dark brown and organics (soft, moist) (TOPSOIL) | xcav. | GROUNDWA | TER |
| | | Sample Number & Interval | Sampler Type | Es = A | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand and | PROFILE Od: Tracked Excavator (ft): Not measured Howard's Construction and Excavator OAR over 7 inches of dark brown and organics (soft, moist) | | GROUNDWA ✓ Perched at 6 feet | TER |
| | | Sample Number & Interval | a Sampler Type | Es = A | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand at | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Excavator OAR over 7 inches of dark brown od organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) | | 7 | TER |
| ; | | Sample Number & Interval | a a Sampler Type | Es = A | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES) Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR over 7 inches of dark brown do organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) | | 7 | TER |
| ; | | Sample Number & Interval | a Sampler Type | Es = A | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand and Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR over 7 inches of dark brown do organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) | | 7 | TER |
| 0 | | Sample Number & Interval | a a Sampler Type | Es = A | | ML ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| 0 | | S-3 Sample Number & S-3 S-4 | a a Sampler Type | Test Data | | ML ML SM | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff or SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| 0 | Elevation (ft) | S-2 Sample Number & State Pit (| and a sampler Type | Es = A | | ML ML SM | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| 0 | Elevation (ft) | S-2 Sample Number & State Pit (| and a sampler Type | W = 33 AL | | ML ML SM | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| | Elevation (ft) | S-2 Sample Number & State Pit (| and a sampler Type | W = 33 AL | | ML ML SM | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| 0 | Elevation (ft) | S-2 Sample Number & State Pit (| and a sampler Type | W = 33 AL | | ML ML SM | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) vistiff, moist) to coarse SAND with gravel | | 7 | TER |
| 0 | Elevation (ft) | S-4 Sent Pit (otal Depth otal Dep | a a Complete Type | W = 33 AL Sted 02/25/20 Pit = 15.0 ft. | | ML ML SM ML | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff or SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) (Brown SILT (very Brown, silty, fine and cobbles (den | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) restiff, moist) to coarse SAND with gravel se, moist) | | 7 | TER |
| 0 | Elevation (ft) | S-4 September 1. Stratig 2. Refere | d d Complete Lype | W = 33 AL Seted 02/25/20 Pit = 15.0 ft. | based | ML ML SM ML SM on field tris neo | Excavation Methor Ground Elevation Excavated By: Logged By: 3 inches of duff of SILT with sand an Mottled orange/b (RECES: Brown, silty, fine (dense, moist) Brown, silty, fine and cobbles (dense) | PROFILE od: Tracked Excavator (ft): Not measured Howard's Construction and Export OAR ver 7 inches of dark brown nd organics (soft, moist) (TOPSOIL) rown/gray SILT (soft, moist) SIONAL LACUSTRINE) to coarse SAND with gravel GLACIAL TILL) restiff, moist) to coarse SAND with gravel se, moist) | | 7 | TER |

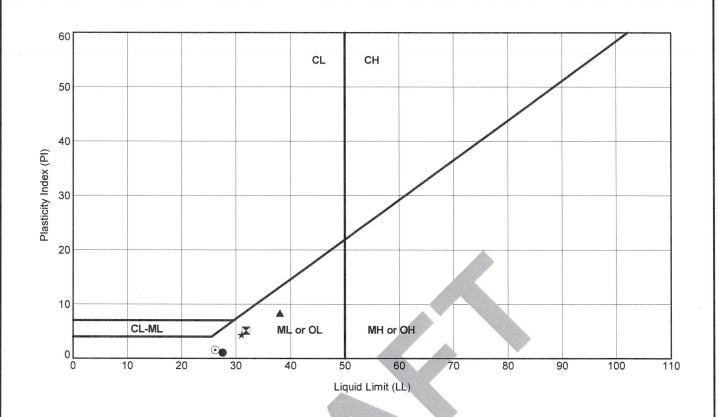
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| SAMPLE DATA | | | | | | | SOIL PROFILE | GROUNDWATER |
|-------------|----------------|-----------------------------|--------------|--------------|----------------|----------------|--|------------------------------|
| | Elevation (ft) | Sample Number & Interval | Sampler Type | Test Data | Graphic Symbol | USCS Symbol | Excavation Method: _Tracked Excavator Ground Elevation (ft): _Not measured Excavated By: _Howard's Construction and Excav. Logged By: _DAR | |
| | | S-1 S-2 | d d | W = 30 AL | | ML ML SM | 4 inches of duff over 10 inches of dark brown SILT with sand and organics (soft, moist) (TOPSOIL) Mottled orange/brown/gray SILT with sand (soft, moist) (RECESSIONAL LACUSTRINE) | Groundwater not encountered. |
| | | S-3 | d | | | | Brown, silty, fine to coarse SAND with gravel (dense, moist) (GLACIAL TILL) Grades to gray at 6 feet | |

Stratigraphic contacts are based on field interpretations and are approximate.
 Reference to the text of this report is necessary for a proper understanding of subsurface conditions.
 Refer to "Soil Classification System and Key" figure for explanation of graphics and symbols.





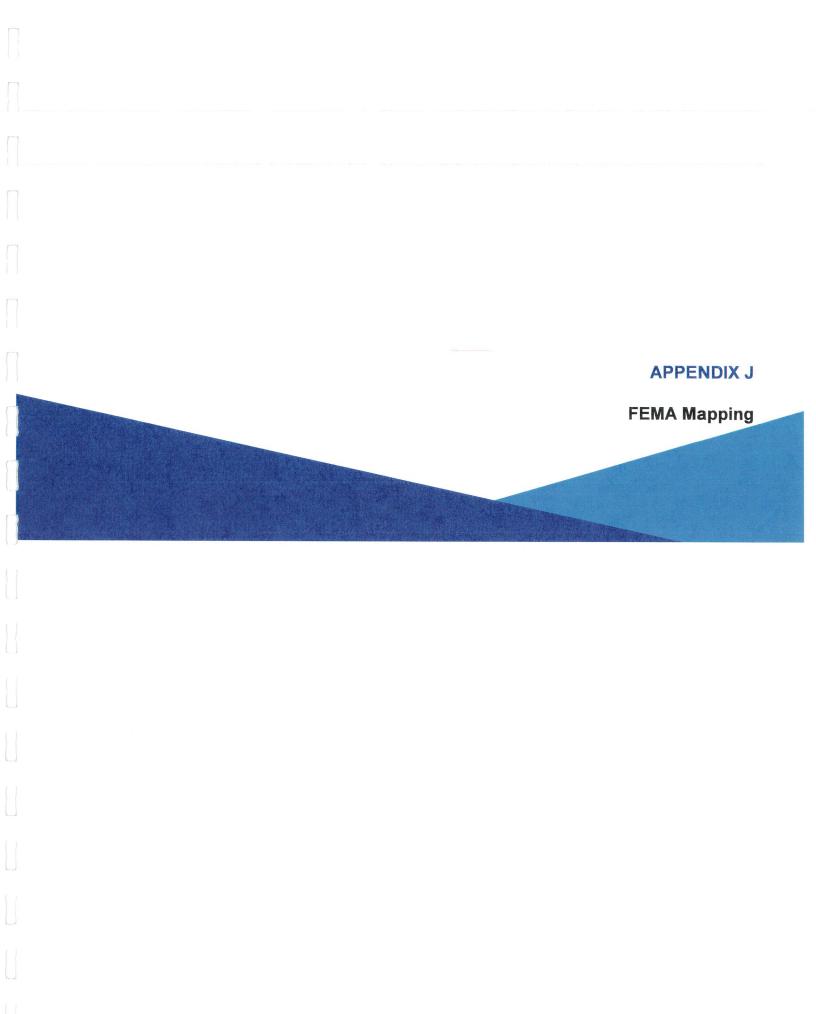


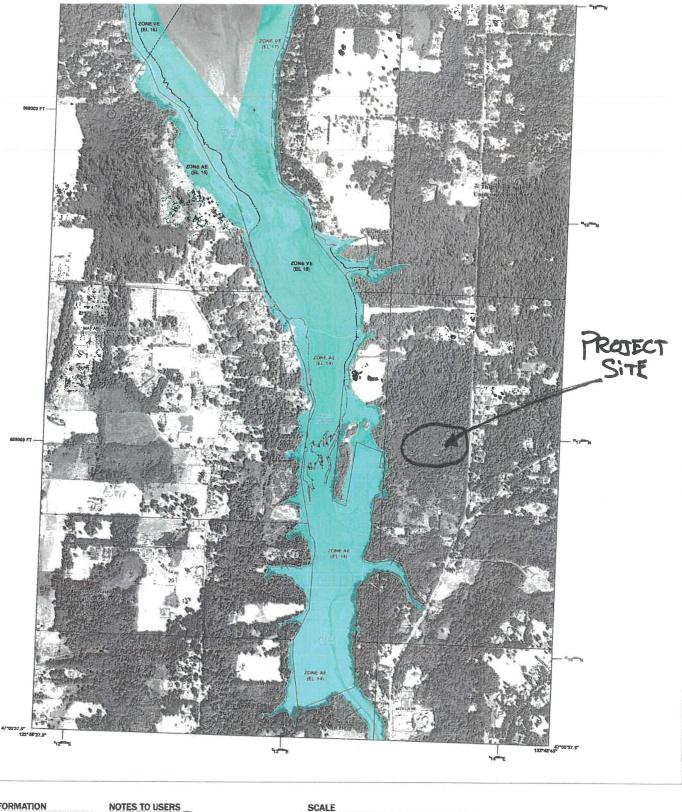
ATTERBERG LIMIT TEST RESULTS

| Symbol | Exploration Number | Sample Number | Depth (ft) | Liquid Limit (%) | Plastic Limit (%) | Plasticity Index (%) | Natural Moisture (%) | Soil Description | Unified Soil Classification |
|----------|-----------------------|------------------|------------|------------------------|-------------------------|----------------------------|----------------------------|------------------|--------------------------------|
| • | TP-1 | S-1 | 2.0 | 28 | 26 | 2 | 28 | SILT with sand | ML |
| × | TP-2 | S-1 | 2.0 | 32 | 27 | 5 | 37 | SILT | ML |
| A | TP-3 | S-1 | 2.0 | 38 | 30 | 8 | 33 | SILT with sand | ML |
| * | TP-4 | S-1 | 2.0 | 31 | 27 | 4 | 33 | SILT | ML |
| • | TP-5 | S-1 | 2.0 | 26 | 25 | 1 | 30 | SILT with sand | ML |

ASTM D 4318 Test Method







FLOOD HAZARD INFORMATION

SEE FIS REPORT FOR DETAILED LEBEND AND INDEX MAP FOR FIRM MANEL LAYOUT THE INFORMATION DEPICTED ON THIS MAP AND SUPPORTING DOCUMENTATION ARE ALSO AVAILABLE HIS DICITAL FORMAT AT HTTP://MSC.FEMA.COV

FLOOD HAZARD

Without Base Flood Elevation (BPE)

Regulatory Floodway

Negatiary recovering 0.2 % Annual Chance Flood Mazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage eneas of less than one square mile <u>Zece X</u> Future Conditions 1% Annual Chance Flood Hazard <u>Zece X</u> Area with Reduced Flood Risk due to Levee See Notes. <u>Zece X</u>

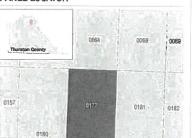
Areas of Minimal Flood Hazard Zone X

Channel, Culvert or Storm S GENERAL STRUCTURES

Non-accredited Levee, Dike or Flo E 18.2 Cross Sections with 1% Annual Chance 177.5 Water Surface Elevations (BFE)

NOTES TO USERS

PANEL LOCATOR



National Flood Insurance Program

NATIONAL FLODD INSURANCE PROGRAM FLOOD INSURANCE RATE MAP

THURSTON COUNTY, WA





Scoping Report Response is on-file with Thurston County

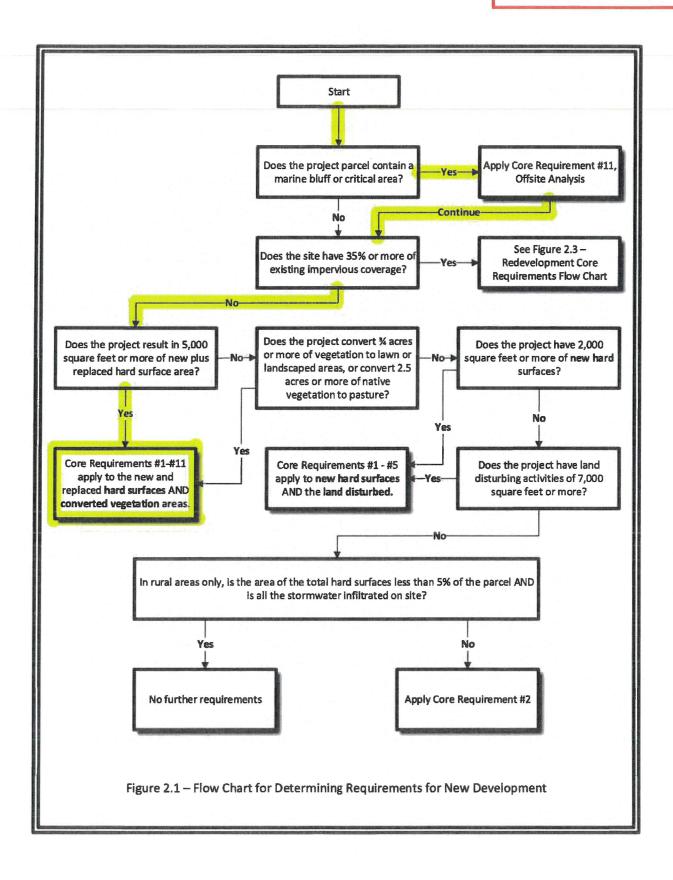


Figure 2-1 Flow Chart for Determining Requirements for New Development.

Checklist LID.11 Full Dispersion

This checklist reflects most, but not necessarily all of the items that will be reviewed by the Development Engineering Section. It is intended to be used as an aid by us to provide a consistent review of development work in Pierce County. All items may not be applicable in the review of each project and all items of concern to this office may not be covered on this checklist.

| Y | N | | |
|---|---|--|--|
| | | MODELING AND SIZING | |
| Y | | Areas that are fully dispersed in accordance with 65/10 Dispersion have fully met Minimum Requirements #5, #6, and #7, and do not need to perform continuous runoff modeling to demonstrate compliance these minimum requirements. | |
| | | DESIGN CRITERIA | |
| | | Setbacks and Site Constraints | |
| Y | | The dispersion of runoff does not create flooding or erosion impacts. | |
| Υ | | The discharge point is not located within 300 feet of erosion hazard, or landslide hazard area. | |
| Υ | | The discharge point is not located within 50 feet from the top of slopes steeper than 20% and greater than 10 feet high. | |
| Υ | | The discharge point is a minimum 30 feet upgradient/ 10 feet downgradient of the drainfield primary and reserve areas. In addition, the flowpath does not intersect with the drainfield primary and reserve area. These requirements can be waived if site topography will clearly prohibit flows from intersecting the drainfield or where site conditions (soil permeability, distance between systems, etc.) indicate that this is unnecessary. | |
| | | General 65/10 Design Criteria | |
| Υ | | Project retains 65% of the site (or a threshold discharge area on the site) in a forested or native condition and impervious developed areas draining to the native vegetation do not exceed 10% of the entire site, or the ratio of the native vegetation area to the impervious area is not less than 65 to 10. | |
| Υ | | The preserved area is placed in a separate tract or protected through recorded easements for individual lots. | |
| Υ | | All trees within the preserved area at the time of permit application are retained, aside from the removal of dangerous or diseased trees. | |
| Υ | | Passive recreation and related facilities do not exceed 8% of the preserved area. | |
| Y | | The preserved area does not include septic systems. | |
| Υ | | Preserved areas are preserved or replanted in accordance with Checklist LID.01 Native Vegetation Protection, Reforestation, and Maintenance. | |
| Y | | Site meets the requirements for: • 65/10 Residential, Commercial, and Industrial Design Criteria (see details below), or • 65/10 Residential, Criteria (see details below) | |
| | | 65/10 Roadway Design Criteria (see details below) 65/10 Residential, Commercial, Industrial Design Criteria | |

Checklist LID.11 Full Dispersion

| Y | N | | | | |
|----------|-----|---|--|--|--|
| | | Applies to site development and roadways planned for urban density | | | |
| | | development. | | | |
| na | | Meets all Design Criteria listed above. | | | |
| | | Lawn and landscaping areas (associated with the development areas) that are dispersed into the native vegetation area meet Volume III, Section 3.1 Soil | | | |
| | | Preservation and Amendment BMP requirements. | | | |
| | | Any additional impervious areas above the 10% do not drain to the native vegetation area. The native vegetation 1 Not Applicable to a set in length (25 feet for sheet) | | | |
| | | The native vegetation 1 Not Applicable to flow from a non-native this project. | | | |
| | | The flowpath is located offsite tract or easement area. | | | |
| | | The slope of the flowpath or dispersal area is no steeper than 15% for any 20-foot reach of the flowpath. If a level spreader is used upstream and vegetation is established, the slope of the flowpath is no steeper than 33%. | | | |
| | | The flowpaths for adjacent dispersion devices are sufficiently spaced to prevent overlap of flows in the flowpath areas. | | | |
| | | Runoff from contributing impervious areas is dispersed into the native vegetation area using the dispersion approaches outlined in the following sections (i.e., Roof Downspout Dispersion, Driveway Dispersion, Roadway | | | |
| \ | | Dispersion, or Cleared Area Dispersion). | | | |
| | 1.5 | Roof Downspout Dispersion | | | |
| na | | Roof surfaces discharge to an area that consists of forested or native vegetative cover and that is more than 65% of the development site area | | | |
| | | (with less than 10% impervious total). | | | |
| na | | Roof downspouts are dispersed in accordance with Downspout Dispersion | | | |
| | | and have flowpaths of 100 feet or more through native vegetation. Driveway Dispersion | | | |
| | - | Driveway surfaces are within a threshold discharge area that is more than | | | |
| na | | 65% forested or native vegetative cover and less than 10% impervious (total). | | | |
| | | Driveway surfaces are dispersed in accordance with Concentrated Flow | | | |
| na | | Dispersion and have flowpaths of 100 feet or more through native vegetation, | | | |
| | | OR driveway surfaces are dispersed along with the road runoff in accordance | | | |
| | | with the roadway dispersion design requirements below. | | | |
| | | Roadway Dispersion | | | |
| Y | | Roadway surfaces are within a threshold discharge area that is more than 65% forested or native vegetative cover and less than 10% impervious (total). | | | |
| | | The road section is designed to minimize collection and concentration of roadway runoff. | | | |
| | | Concentrated flows are incrementally discharged from the ditch via cross culverts or at the ends of cut cross-sections at a maximum rate of 0.5 cfs for | | | |
| | | the peak 100-year flow. For discharge locations with up to 0.2 cfs for the peak 100-year flow, rock | | | |
| + | | pads or dispersion trenches are used to disperse flows. For discharge locations with between 0.2 and 0.5 cfs discharge for the 100- | | | |
| • | | year peak flow, dispersion trenches are used to disperse flows. | | | |
| | | | | | |

(D.11 sion

| 1 | | SIUII |
|----------|---|--|
| Y | N | |
| n/a | | If included, dispersion trenches meet the following design criteria: Designed to accept surface flows (free discharge) from a pipe, culvert, or ditch end and aligned perpendicular to the flowpath |
| | | Minimum of 2 feet wide by 2 feet deep |
| | | Minimum of 50 feet in length |
| | | • Filled with 0.75-inch to 1.5-inch washed rock |
| | | Minimum spacing of 50 feet between centerlines |
| Υ | | Flowpaths from adjacent discharge points do not intersect within the 100-foot flowpath lengths, and dispersed flow from a discharge point is not intercepted by another discharge point. |
| Υ | | There is no county-determined potential for significant downstream impacts. |
| | | Cleared Area Dispersion |
| | | Cleared areas draining to the dispersion areas consist of bare soil, non-native |
| na | | landscaping, lawn, or pasture. |
| | | Runoff from the cleared area is dispersed through at least 25 feet of native vegetation. Not Applicable to |
| | | No more than 25 feet in contributhis project, through the |
| | | cleared area). The dispersal flov 1 foot for every 3 |
| | | feet of contributing flowpath beyond 25 rect (up to a maximum contributing |
| | | flowpath of 250 feet). |
| | | The topography of the non-native pervious surface does not allow runoff to |
| \ | | concentrate prior to discharge to the dispersal area. |
| | | 65/10 Roadway Project Design Criteria Applies to public and private roads, typically on roads outside of the urban |
| | | growth areas. |
| | | Uncollected or Natural Dispersion into Adjacent Vegetated Areas |
| | | (i.e., sheet flow into the dispersion area) |
| Υ | | Depth to the average annual maximum groundwater elevation is at least 3 feet. |
| 1 | | The contributing impervious surface flowpath length is less than 75 feet. |
| | | The contributing pervious flowpath length is less than 150 feet. |
| | | The lateral slope of contributing impervious drainage area is less than 8%. |
| | | The longitudinal slope of road is less than 5%. |
| | | |
| | | Road side slopes (not part of the dispersion area) are less than 25%. |
| | | Dispersion area does not include road side slopes unless native vegetation is re-established and slopes are less than 15%. |
| | | Road shoulders that are paved or graveled are counted as impervious surface. (Permeable pavement shoulders are considered a hard surface, not an impervious surface.) |
| | | |
| | | The length of the dispersion area is equivalent to length of road. |
| | | The length of the dispersion area is equivalent to length of road. The average longitudinal (parallel to road) slope of the dispersion area is less than 15%. |

Checklist LID.11 Full Dispersion

| Y | N | Tun Dispersion | | | |
|----------|----|--|--|--|--|
| - | 11 | For sites with outwash soils with initial hydraulic conductivity of 4 inches per | | | |
| | | hour or greater, the following criteria are met: | | | |
| | | | | | |
| na | | • 10 feet of dispersion area flowpath is provided for up to 20 feet of | | | |
| | | contributing impervious width (i.e., perpendicular to the direction of | | | |
| | | roadway travel). | | | |
| 1 | | • Each additional foot of contributing impervious width includes an | | | |
| | | additional 0.25 feet of dispersion area flowpath. | | | |
| | | For sites with soils not meeting the above criteria (Types C and D, and some | | | |
| | | Type B), the following criteria are met: | | | |
| Y | | • 6.5 feet of flowpath is included for every 1 foot of contributing | | | |
| | | impervious width draining to it. | | | |
| | | A minimum flow path distance of 100 feet is provided. | | | |
| | | Channelized Stormwater Into Areas With a) Native Vegetation or b) | | | |
| | | Cleared Land in Areas Outside of the UGA | | | |
| Υ | | Depth to the average annual maximum groundwater elevation is at least 3 | | | |
| • | | feet. | | | |
| Y | | Channelized flow is re-dispersed to produce the longest possible flowpath. | | | |
| | | | | | |
| Υ | | Flows are evenly dispersed across the dispersion area. | | | |
| Υ | | The length of dispersion area is equivalent to length of the road. | | | |
| | | The average longitudinal and lateral slopes of the dispersion area are less | | | |
| | | than 8%. | | | |
| | | The slope of any flowpath segment is no steeper than 15% for any 20-foot | | | |
| | | reach of the flowpath segment. | | | |
| | | Flows are dispersed using rock pads and dispersion techniques as specified | | | |
| | | under Roadway Dispersion (see above). | | | |
| | | For sites with outwash soils with initial hydraulic conductivity of 4 inches per | | | |
| | | hour or greater, the dispersion area flowpath is at least half the width of the | | | |
| | | contributing impervious drainage area. | | | |
| | | For sites with soils not meeting the above criteria (Types C and D, and some | | | |
| | | Type B), the following criteria are met: | | | |
| | | • 6.5 feet of flowpath is included for every 1 foot of contributing | | | |
| | | impervious width draining to it. | | | |
| ↓ | | A minimum flow path distance of 100 feet is provided. | | | |
| | - | | | | |
| | | Engineered Dispersion of Stormwater Runoff into Areas with Engineered Soils | | | |
| | | Depth to the average annual maximum groundwater elevation is at least 3 | | | |
| | | feet | | | |
| - | | Average longituding this project of dispersion area is less than | | | |
| | | Average longituding this project. Not Applicable to of dispersion area is less than of dispersion area is less than | | | |
| - | | Average lateral slop ss than 15%. | | | |
| | | | | | |
| | | The dispersion area is planted with native trees and shrubs. | | | |

Checklist LID.11 Full Dispersion

| Y | N | |
|---|------|--|
| | | Stormwater is dispersed via sheet flow or via collection and re-dispersion in accordance with the techniques specified under Roadway Dispersion (see above). |
| | | For sites with outwash soils with initial hydraulic conductivity of 4 inches per hour or greater, the following criteria are met: Soil are amended to meet Volume III, Section 3.1 Soil Preservation and Amendment BMP requirements. 10 feet of dispersion area flowpath is provided for up to 20 feet of impervious width. An additional 0.25 feet of dispersion area flowpath is provided for each additional foot of impervious width beyond 20 feet. For sites with soils not meeting the above criteria (Types C and D, and some Type B), the following criteria are met: Soil are amended to meet Volume III, Section 3.1 Soil Preservation and |
| | | Amendment BMP requirements. • The dispersion area must meet the 65/10 ratio. |
| | | CONSTRUCTION CRITERIA INCLUDED IN THE SWPPP |
| | | The preserved area is shown on all property maps. |
| | | The dispersion area is clearly identified (e.g., using flagging or high visibility fencing) and protected prior to and during construction. |
| | | A soil and vegetation sweep Not Submitted for the dispersion area Construction SWP The dispersion area Construction SWP The dispersion area Construction SWP The dispersion area Sweep The dispersion |
| | | Construction SWPPP BMPs and protection techniques are implemented as applicable. The upslope of construction areas are stabilized and overland flow distances are minimized. |
| | | Operate machinery outside of dispersion area during construction. |
| | | Refer to construction requirements in Checklist 42: Preserving Native |
| | | Vegetation and Restoring Site Vegetation. |
| | 5 80 | INSPECTION CRITERIA |
| | | The dispersion facility meets applicable design and construction criteria (see * in Design Criteria above). |

